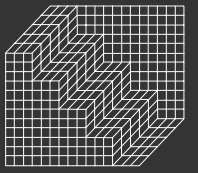




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Joint Component Behaviour in Fire

Florian M. Block

Ian W. Burgess

J. Buick Davison

Steel in Fire Forum

Rotherham, UK

September 2004

Beam and Joint Forces in Fire

Beam:

Bending

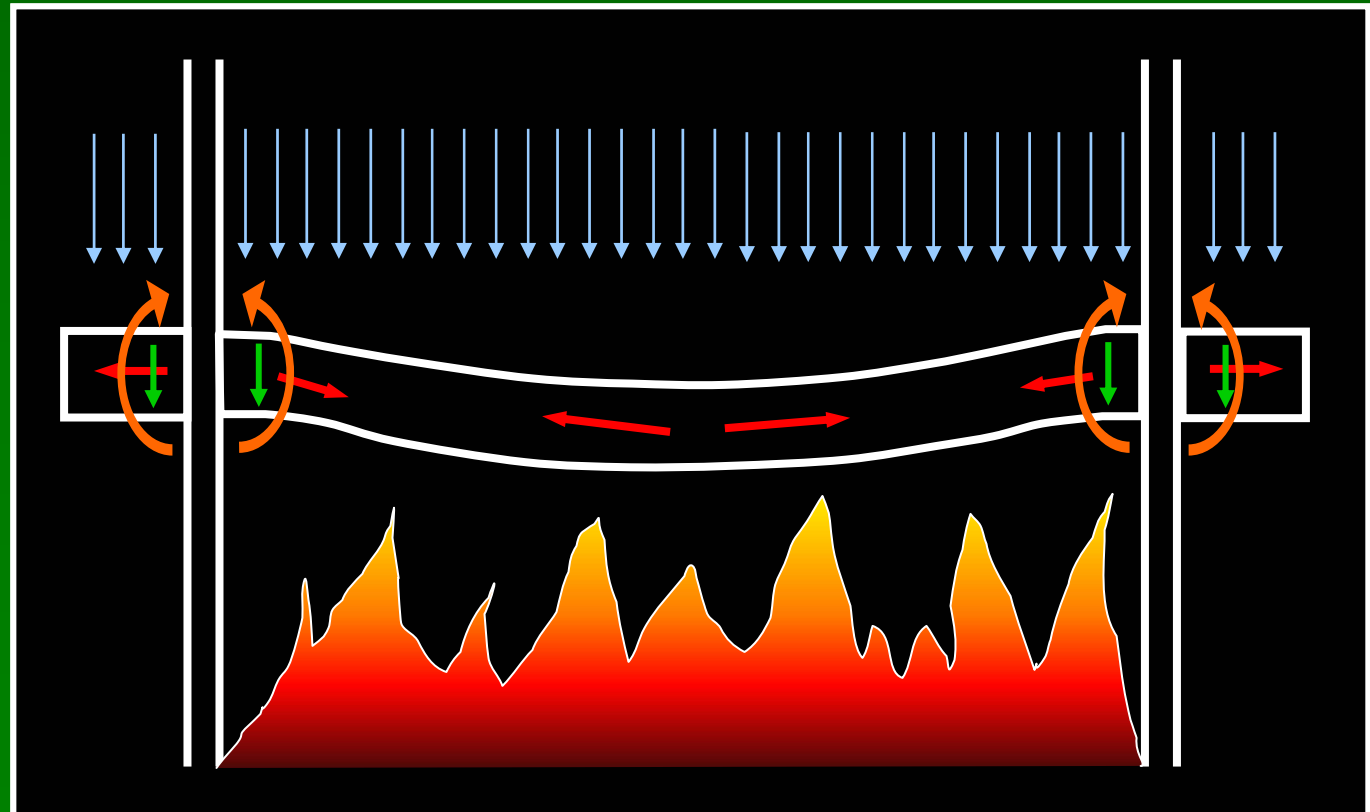
Joint:

Shear

Bending and Compression Shear, Bending and Compression

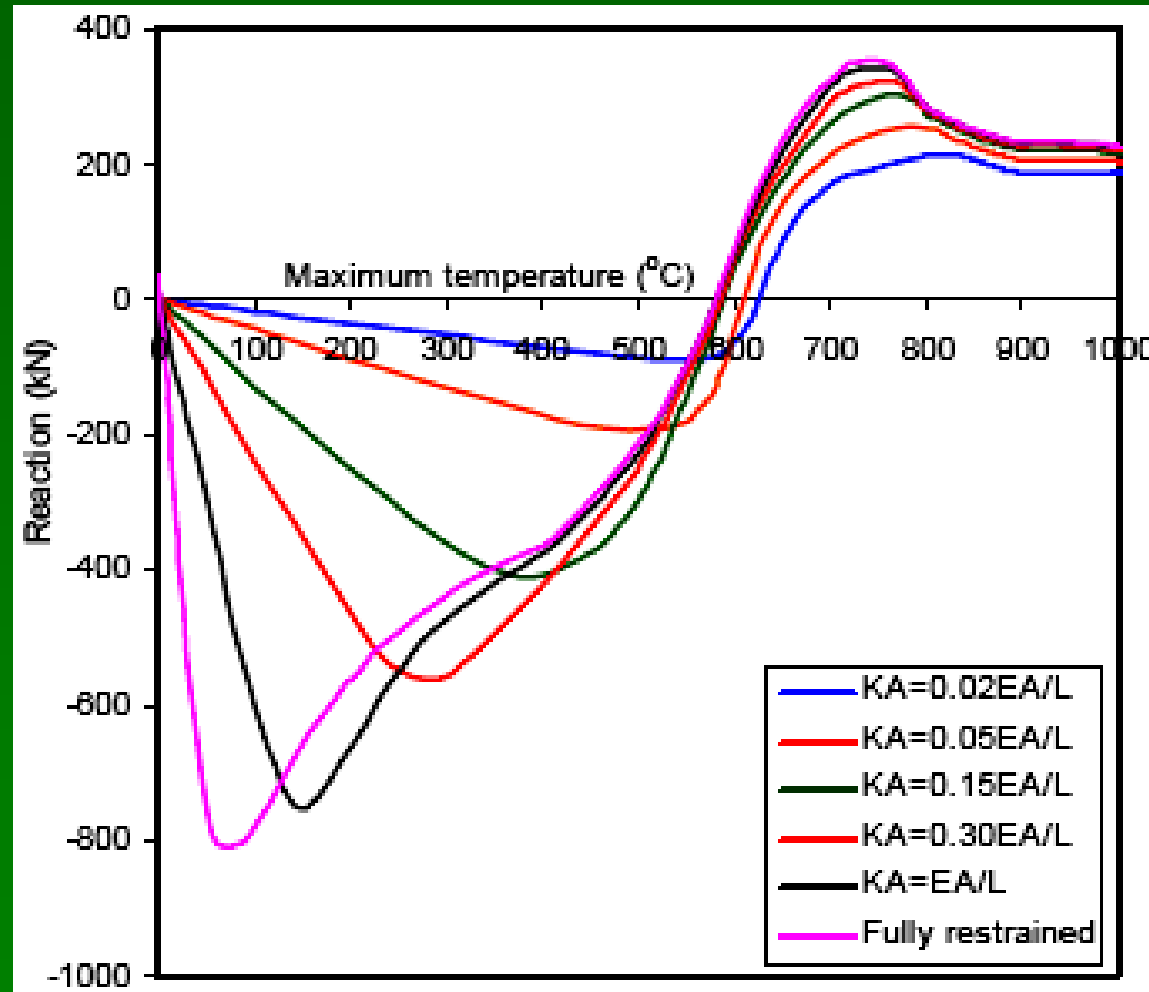
Tension

Shear, Bending and Tension

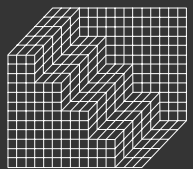


Axial Beam Forces in Fire

Axial beam forces depend on the axial joint stiffness.



by Y.Z. Yin, Manchester Centre for Civil and Construction Eng.



Cardington Beam-Column Joint after Fire Test # 7

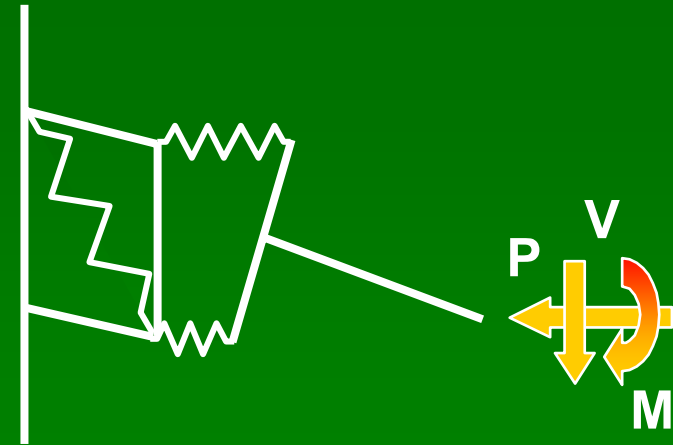
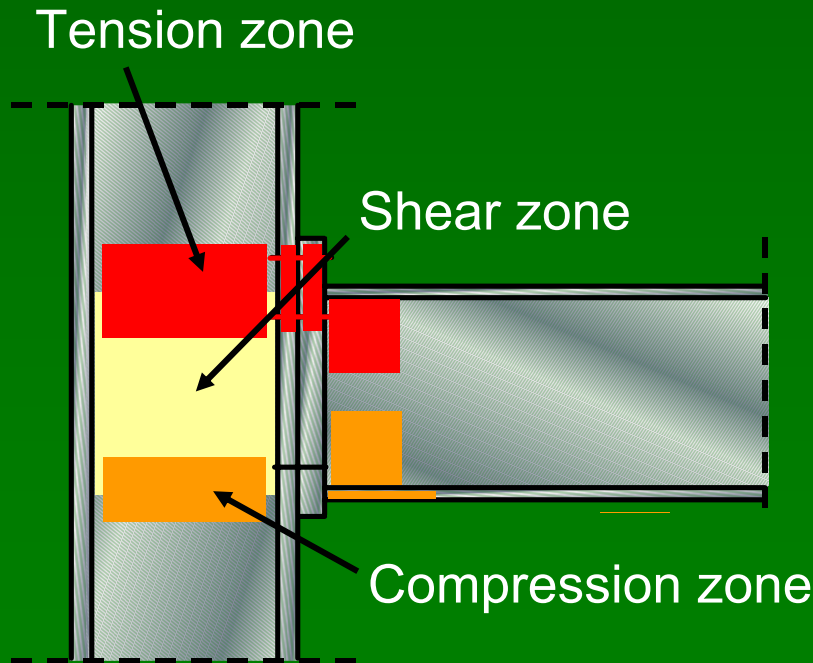


Beam shear buckling

Beam flange buckling

The Component Method

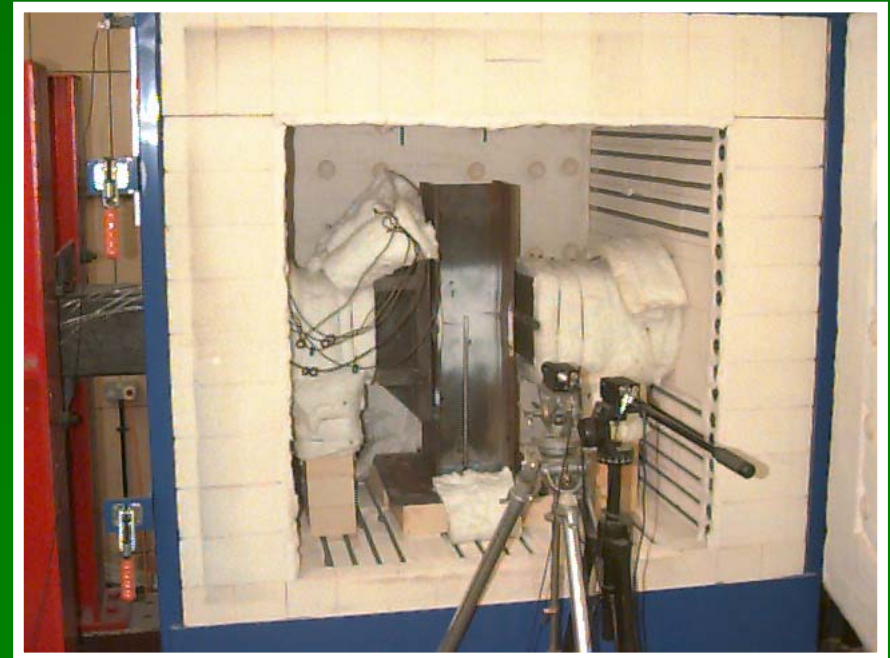
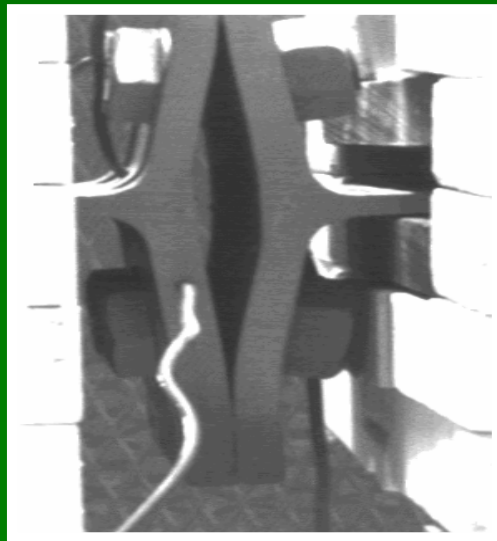
- A flexible approach based on modelling the zones of fundamental behaviour (“components”) within a joint.
- Reassembling a model of the joint with springs.



What has been done before?

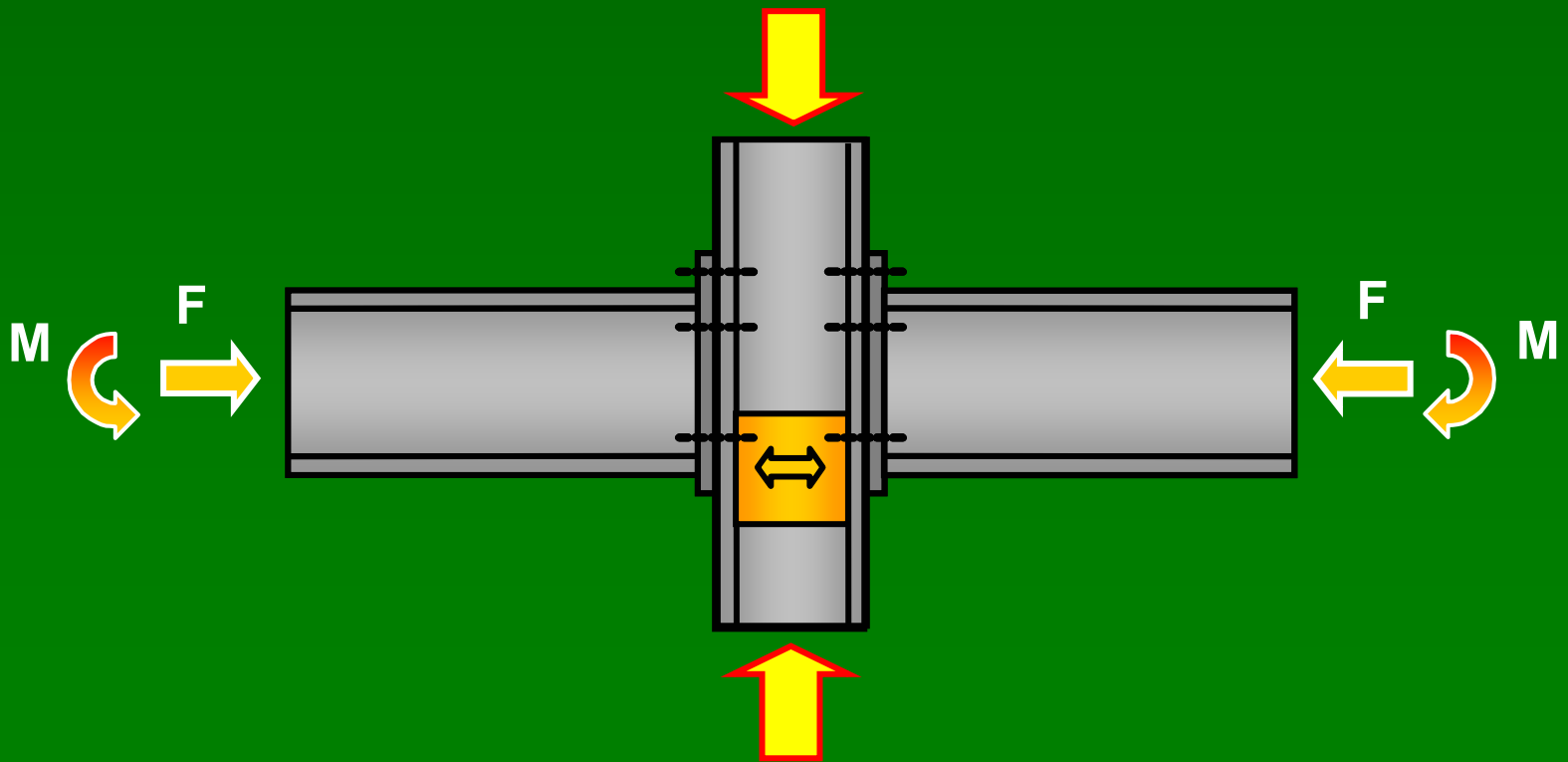
Experimental test program and analytical / semi-empirical models by S. Spyrou (1998 – 2001) at the University of Sheffield:

- Tension zone of endplate joints as T-Stub
- Compression zone in the column web



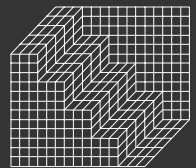
Compression Zone: Column Web

- Can become critical at a relatively early stage of fire due to thermal expansion of the beams.
- Can cause column buckling by forming a plastic hinge in the column and increasing the buckling length.





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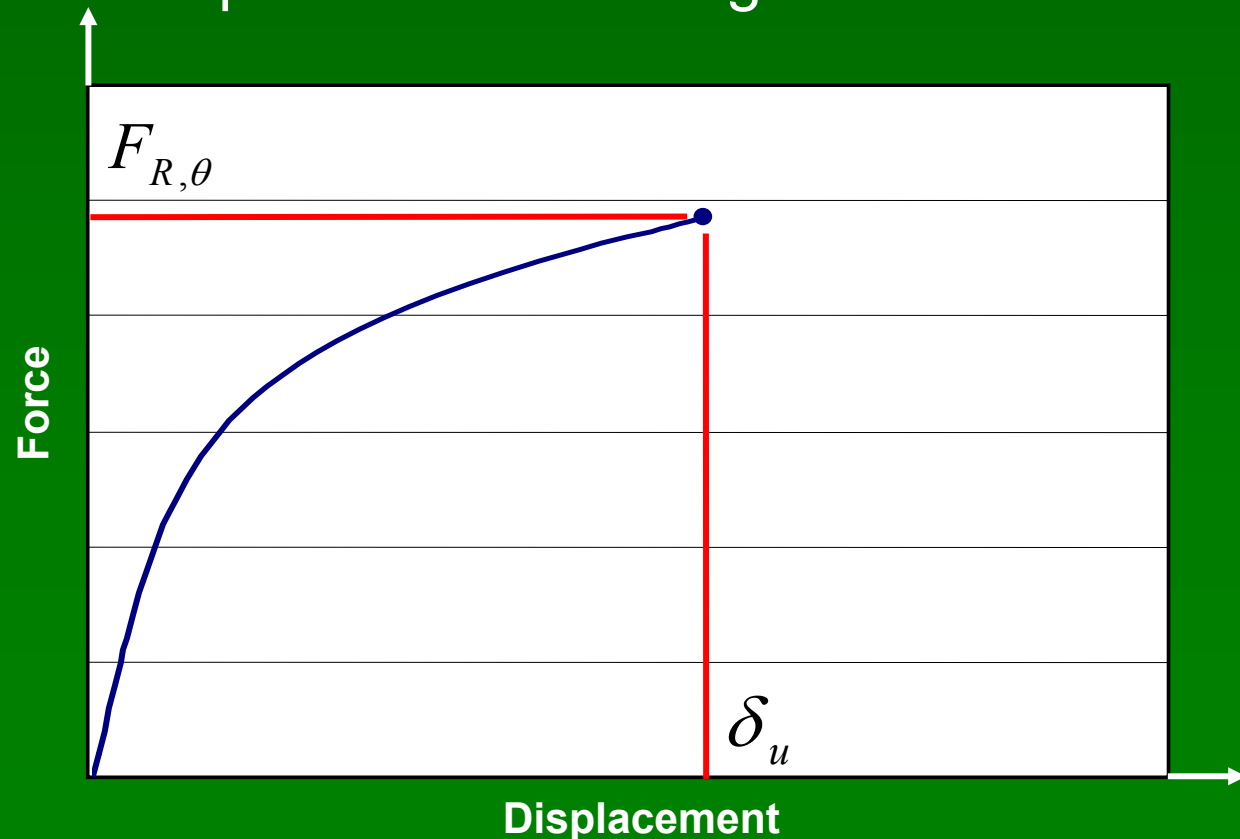


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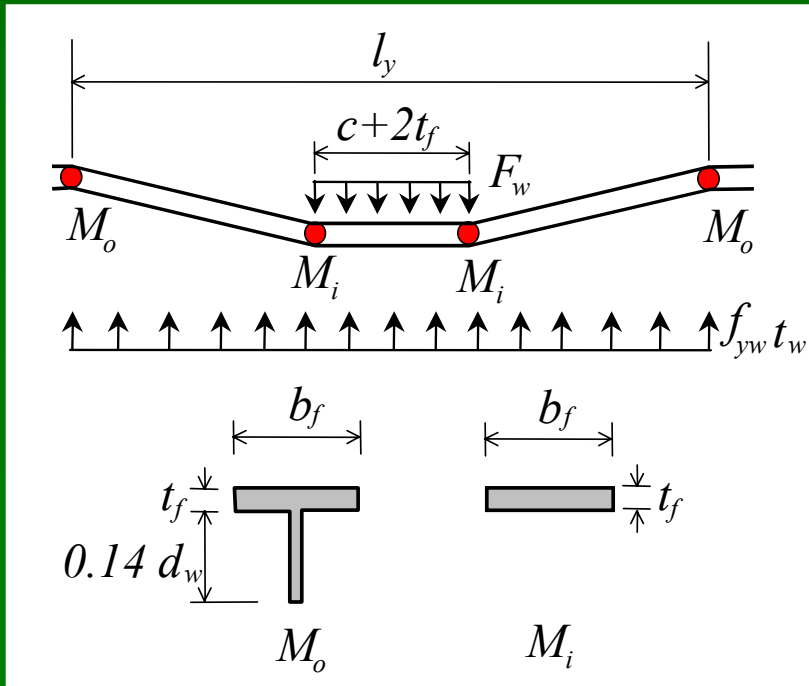
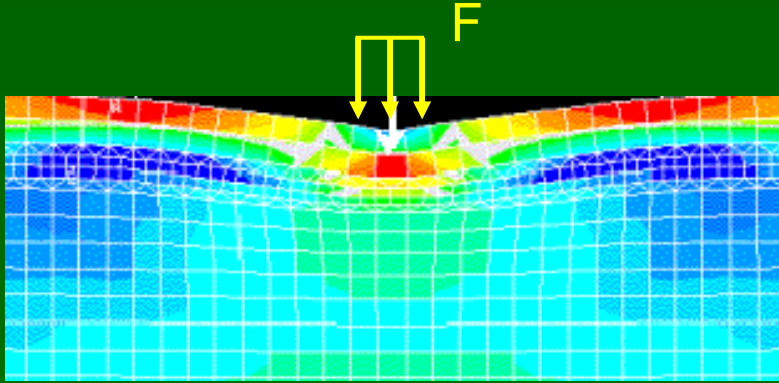
Force – Displacement Model...

Force – Displacement Model for the Compression Zone

1. Ultimate strength
2. Displacement at ultimate strength
3. Curve up to ultimate strength



1. Lagerqvist – Equation for the Ultimate Strength



$$F_{R,\theta} = k_{y,\theta} f_{yw} L_{eff} t_w$$

$$L_{eff} = \chi_F l_y$$

$$\chi_F = \frac{0.5}{\lambda_F} \leq 1.0$$

$$\lambda_F = \sqrt{\frac{l_y t_w k_{y,\theta} f_{yw}}{F_{cr}}}$$

$$F_{cr} = k_F \frac{\pi^2 k_{E,\theta} E}{12(1-\nu^2)} \frac{t_w^3}{d_w}$$

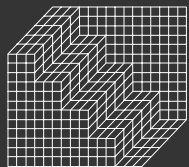
with $k_F = 3.5$

2. Numerical Study of the Peak Displacement

A 3D ANSYS Finite Element Model was used to perform a parametric study of the displacement at ultimate strength.

Parameters studied:

Web thickness	$t_w = 4 - 11$ mm
Web depth	$d_w = 95 - 271$ mm
Yield stress	$f_y = 235 - 460$ N/mm ²
Flange thickness	$t_f = 4 - 15$ mm
Load introduction width	$c = 12 - 96$ mm





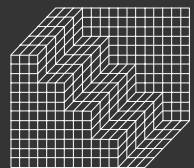
2. & 3. Displacement of the Compression Zone

Equation for the displacement at ultimate strength as found in the parametric study:

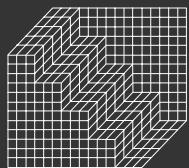
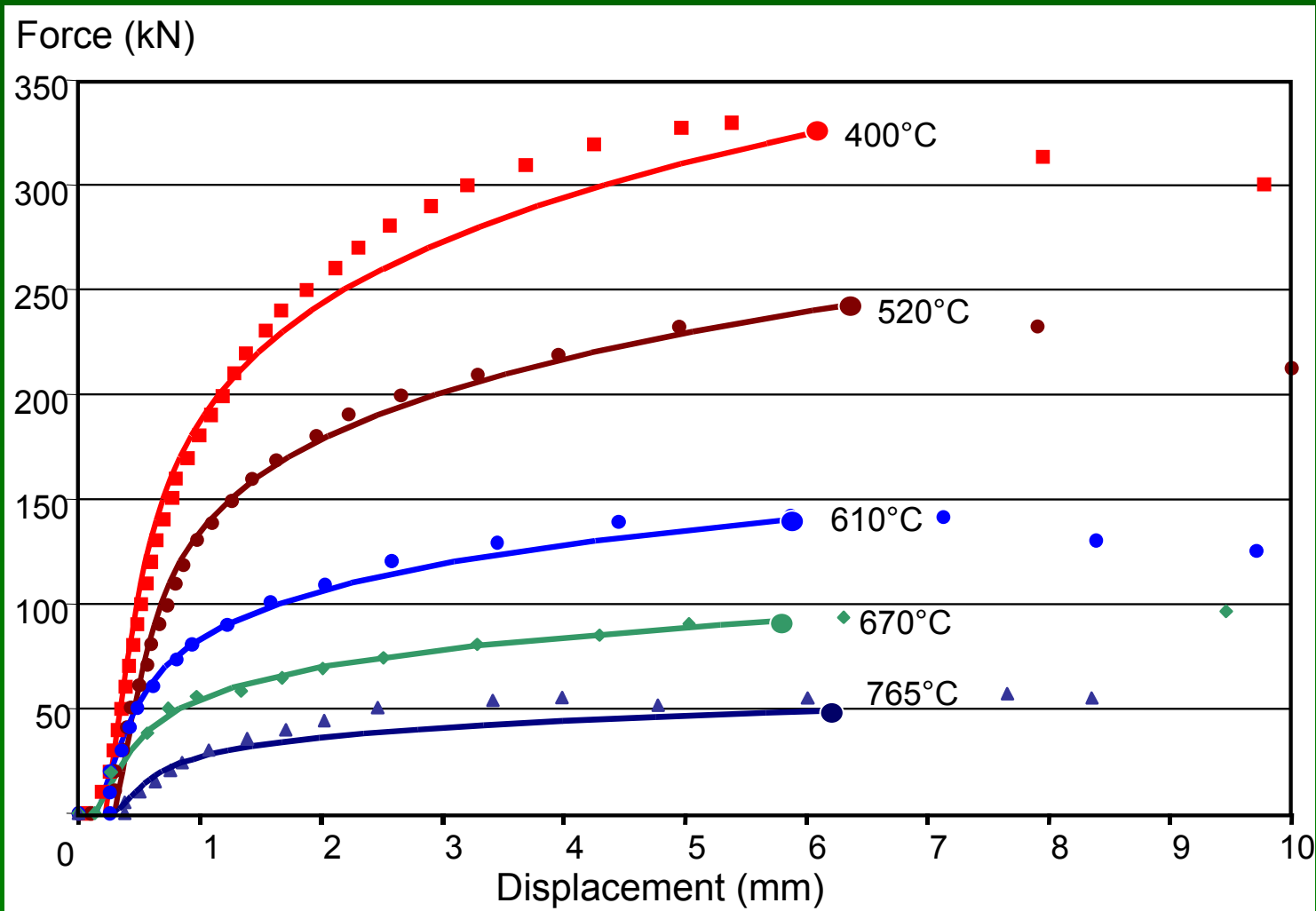
$$\delta_{u,pl} = 0.25 \frac{l_y t_w^2}{b_f t_f} \sqrt{\frac{t_w}{t_f} \frac{d_w}{c}}$$

Modified Ramberg-Osgood equation including the initial stiffness of EC3 Part 1.8 for the compression zone:

$$\delta_i = \frac{F_i d_w}{0.7 k_{E,\theta} E l_y t_w} + \delta_{u,pl} \left(\frac{F_i}{F_{R,\theta}} \right)^5$$

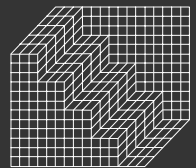


Comparison of the Analytical Model with Test results





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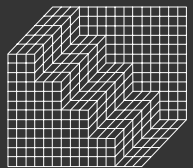


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Influence of Axial Load...

Influence of Axial Load in the Column

- Tests at 20°C have shown that axial load in the column reduces the resistance and the deformation capacity.
- All existing reduction factors are based on ambient temperature experiments.
- A FEM Study has been conducted and an experimental programme at high temperatures is in progress.

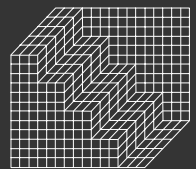
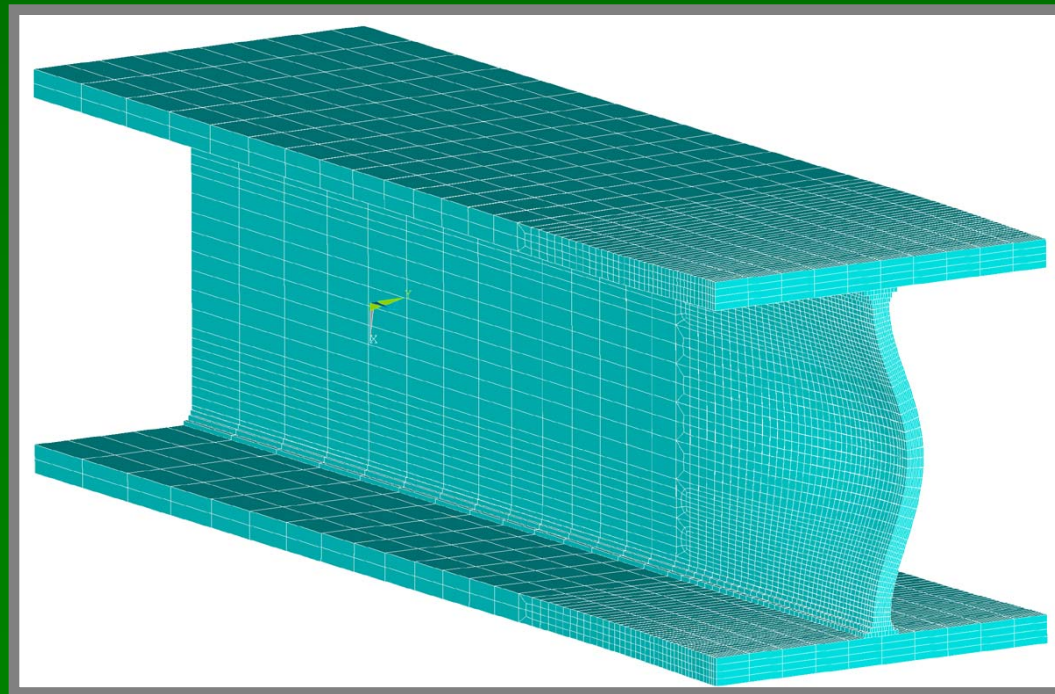




- ANSYS Layered Thin-Shell-Elements
- 3 British column sections with d_w / t_w between 10.4 and 22.3

FEM Model

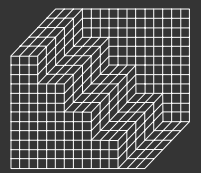
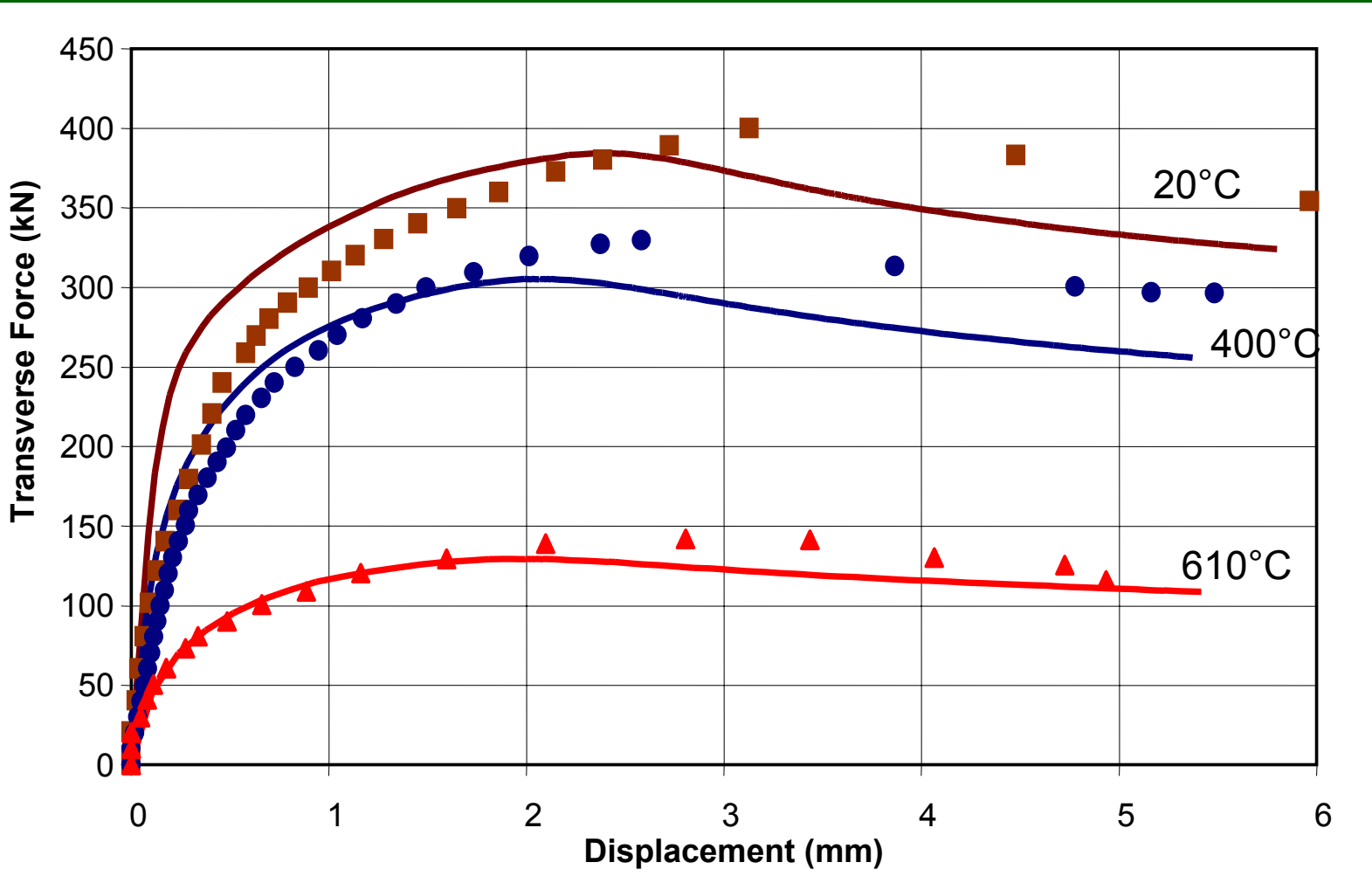
- Uniform temperatures up to 650°C
- Material properties from EC3 Part 1.2
- Axial loads up to 80% of the effective yield load



Comparison between the FEM Model and Test Results



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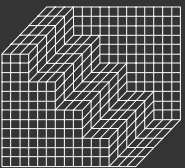


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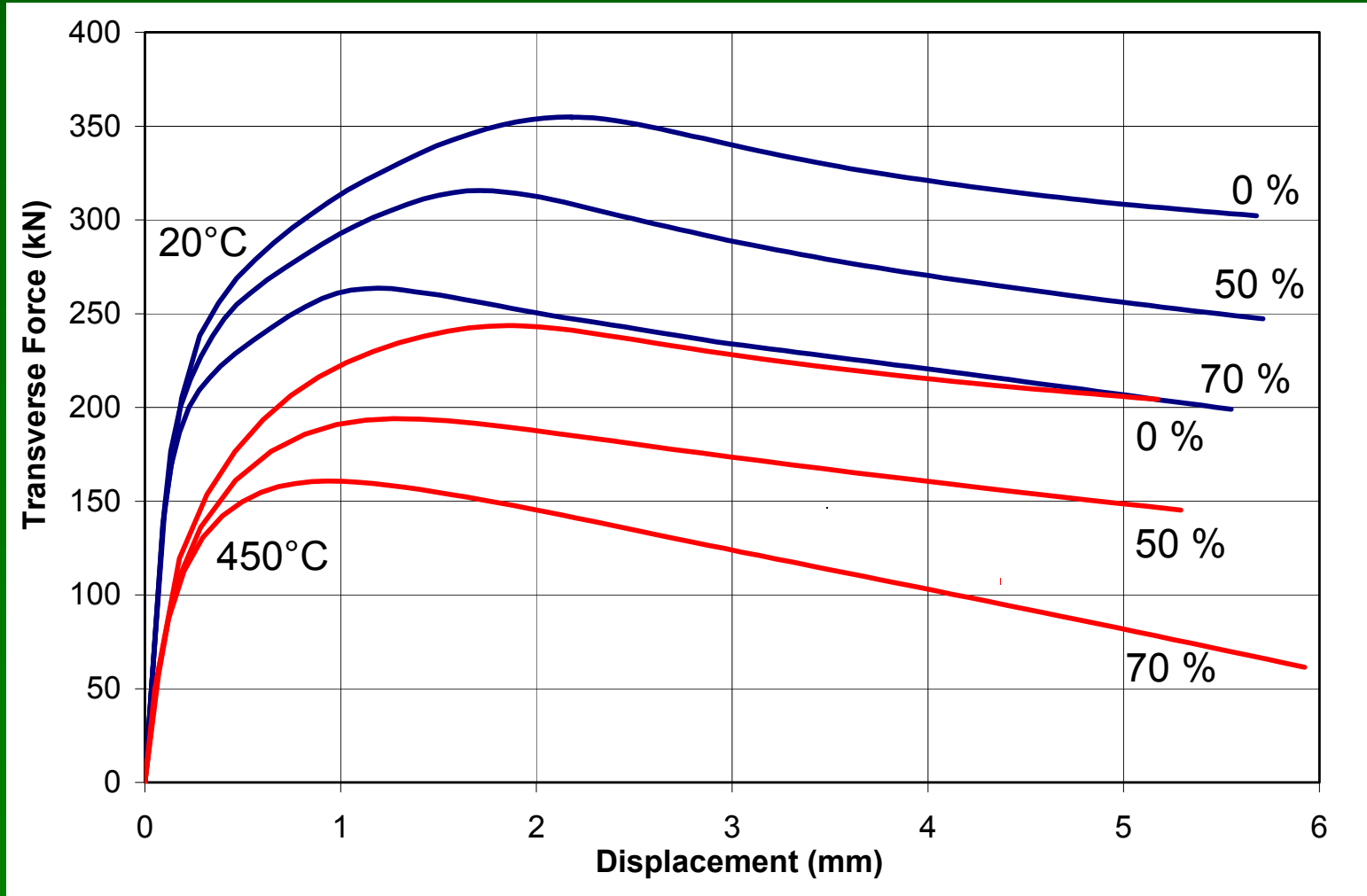
Influence of the Axial Load



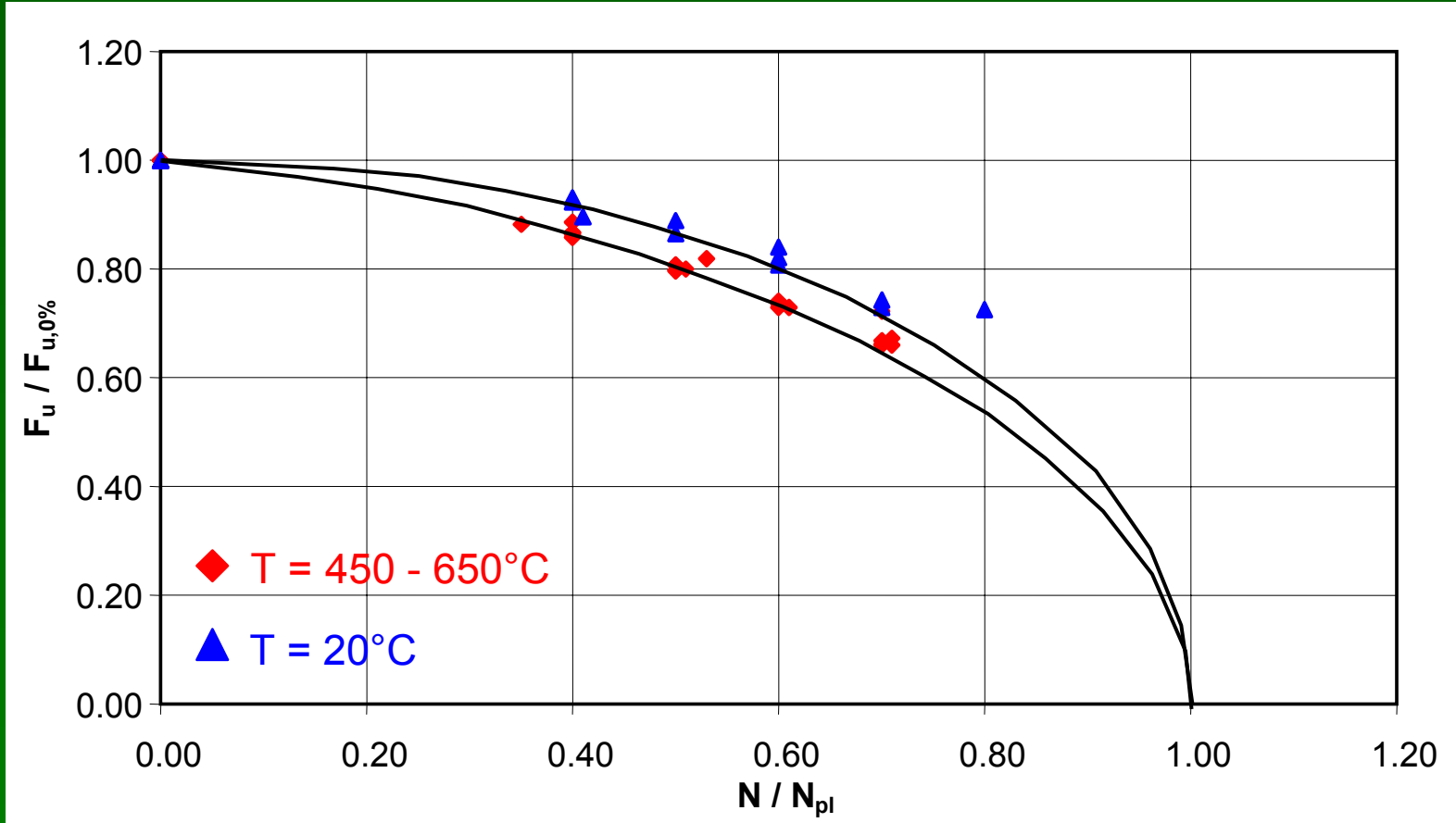
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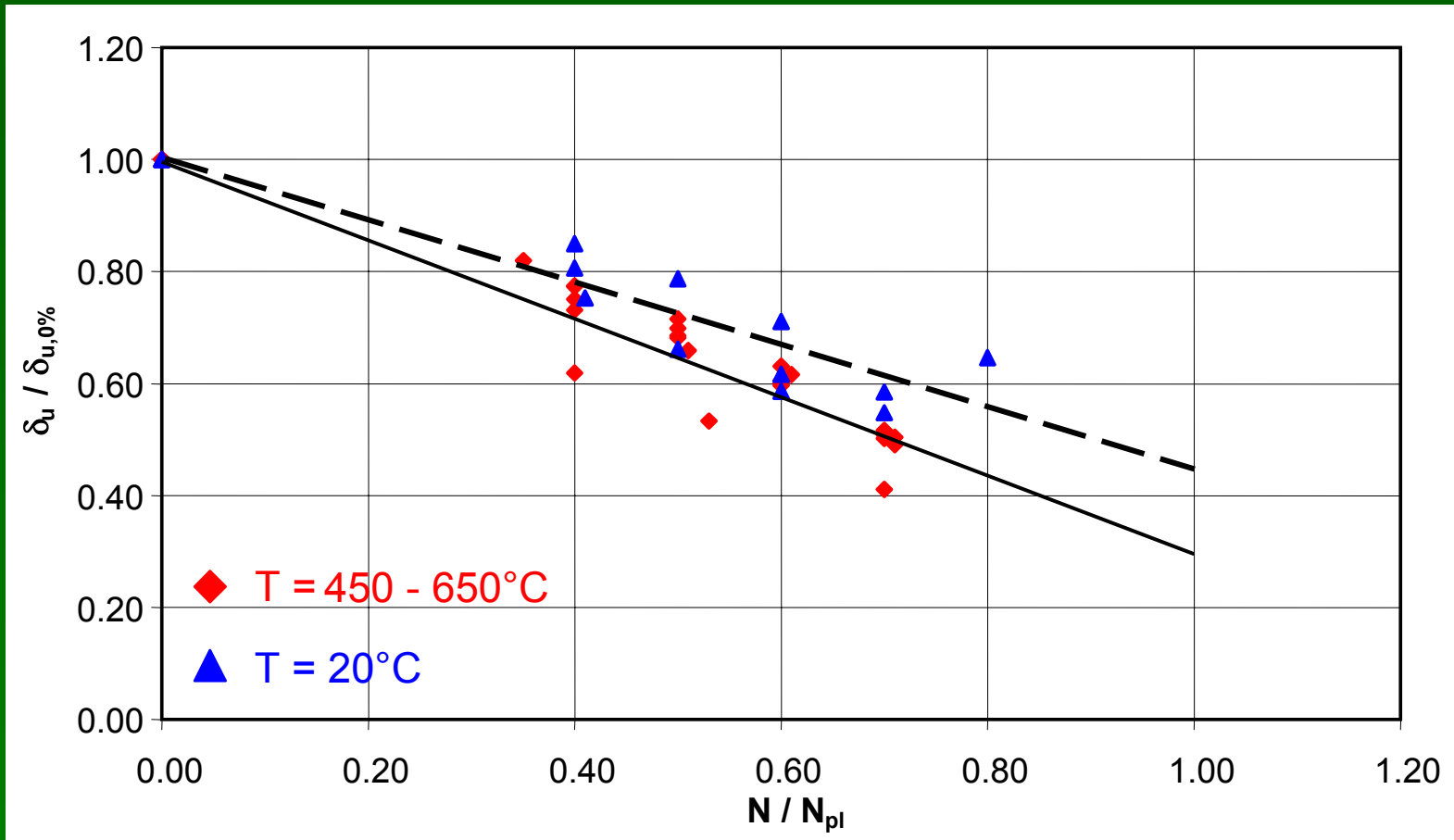
Reduction of the Ultimate Strength



$$k_{N,20^\circ\text{C}} = \sqrt{1 - \left(\frac{\sigma_N}{f_{y,w}} \right)^2}$$

$$k_{N,\geq 400^\circ\text{C}} = \sqrt{1 - \left(\frac{\sigma_N}{k_{y,\theta} f_{y,w}} \right)^{1.55}}$$

Reduction of the Displacement



$$k_{N,\delta,20^{\circ}\text{C}} = -0.55 \frac{\sigma_N}{f_{y,w}} + 1$$

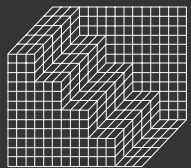
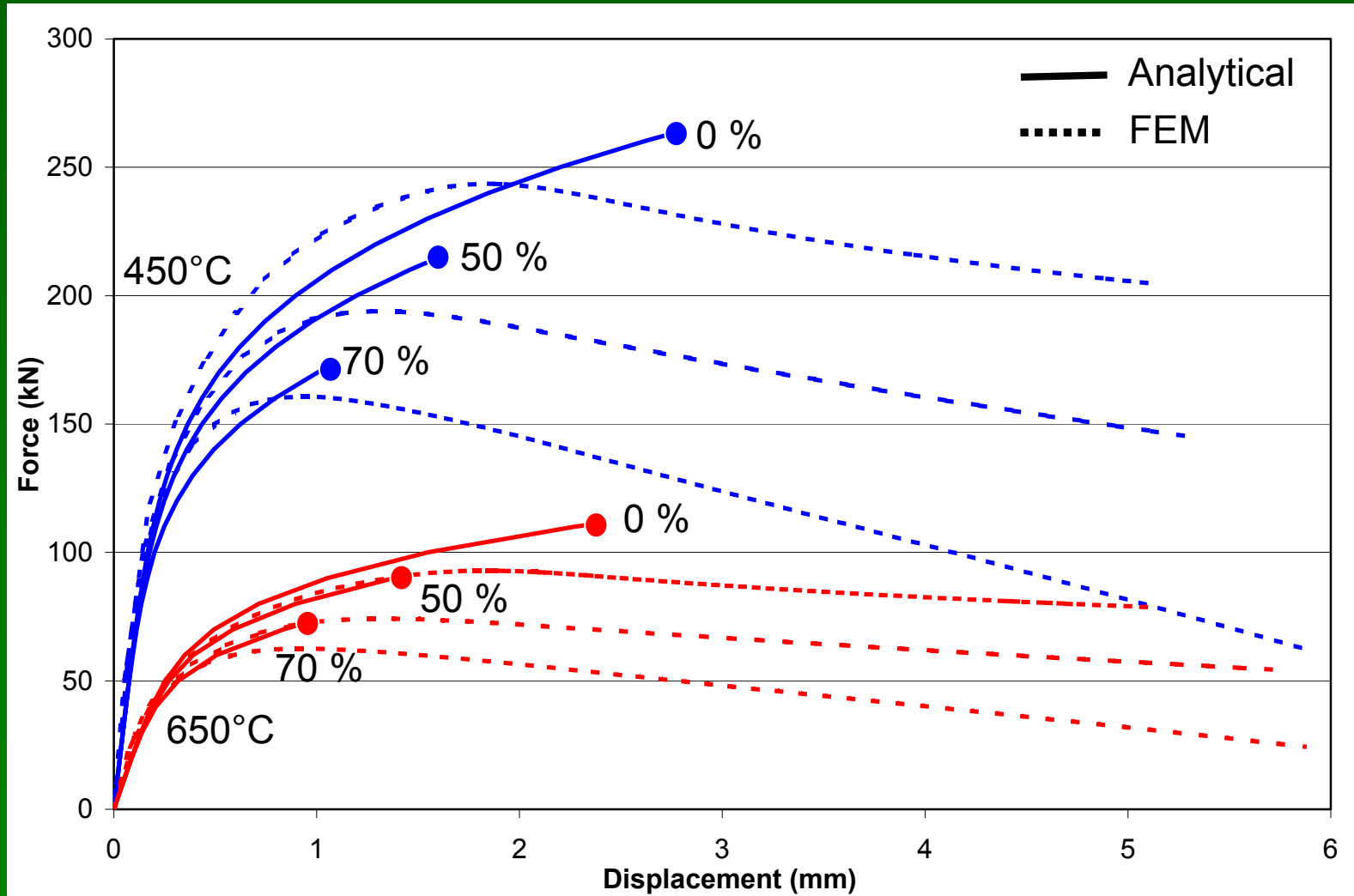
$$k_{N,\delta,\geq 400^{\circ}\text{C}} = -0.70 \frac{\sigma_N}{k_{y,\theta} f_{y,w}} + 1$$



Analytical Model with Reduction Factors compared with FEM Model



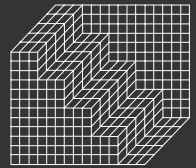
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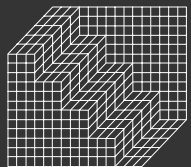


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Experimental Work...

Experimental Objectives

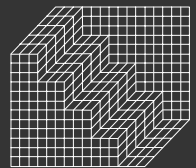
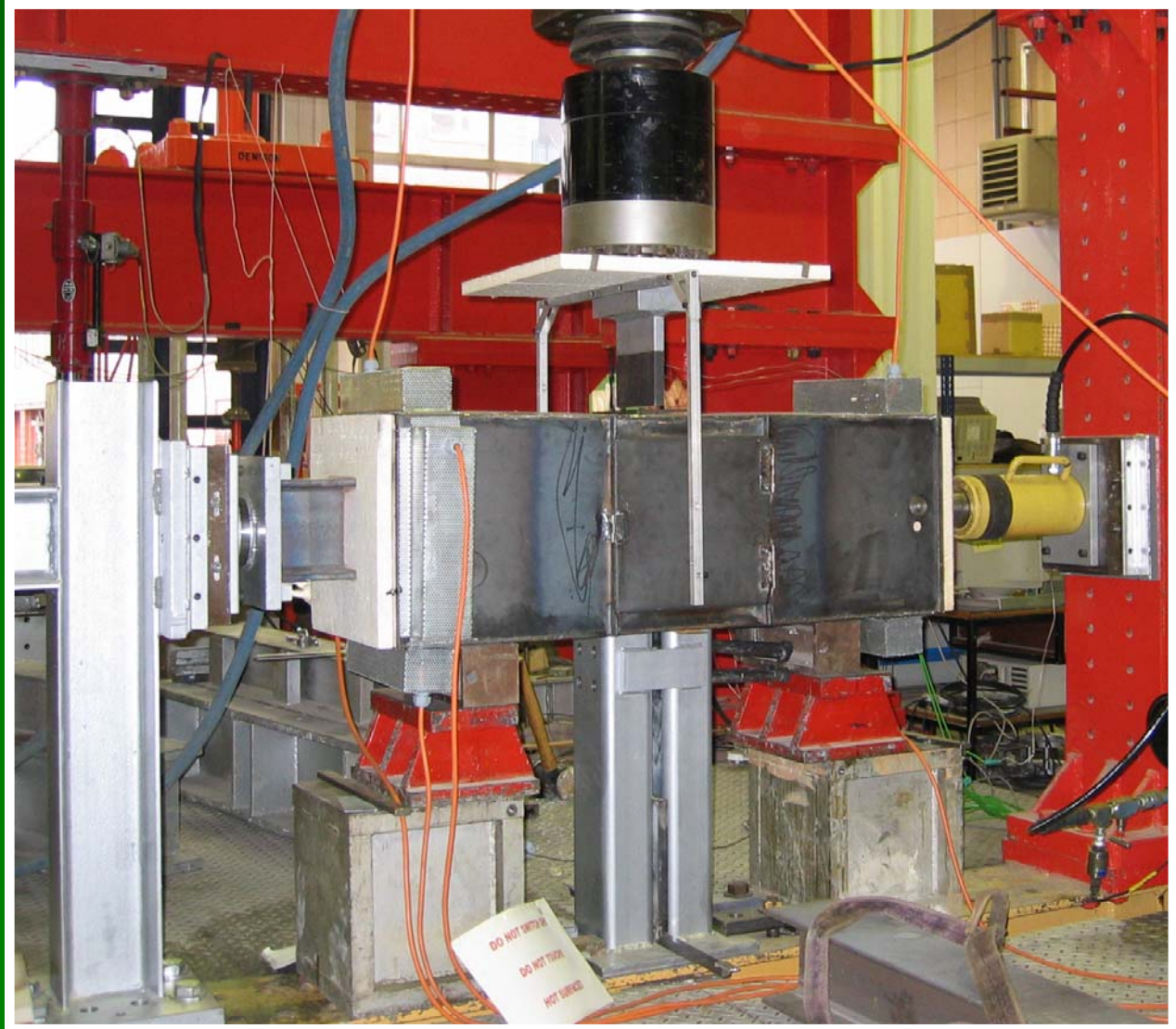
- The influence of the axial load on the compression zone is based on numerical calculations only.
- Not a full experimental study - only for validation of numerical analysis.
- 12 tests at 4 different temperatures and 3 different axial load ratios.
- Isothermal / steady-state tests
- Specimen: UC 152x152x37 Grade S275



Overview of the Experimental Setup



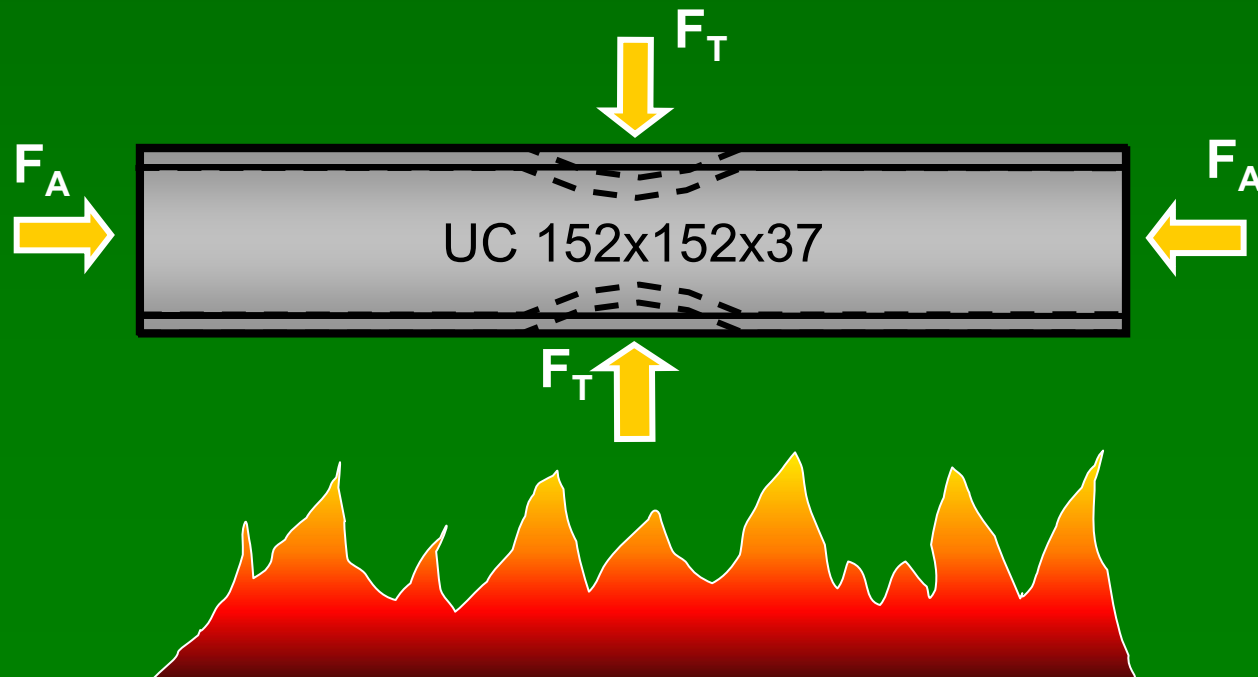
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Test Procedure

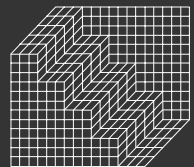
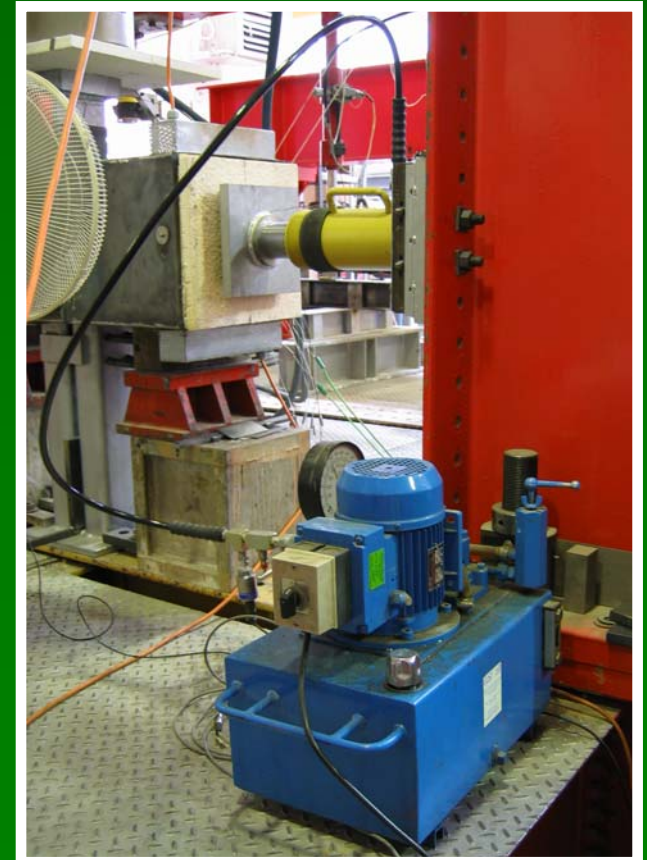
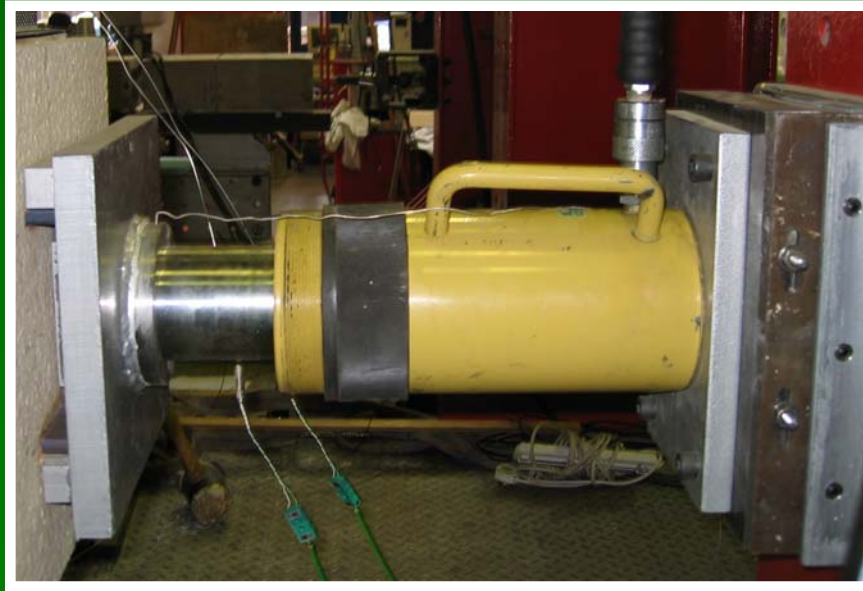
1. Axial loading of the specimen to simulate the super-load in the column.
2. Heating of the specimen up to test temperature.
3. Transverse loading of the specimen until failure of the compression zone.





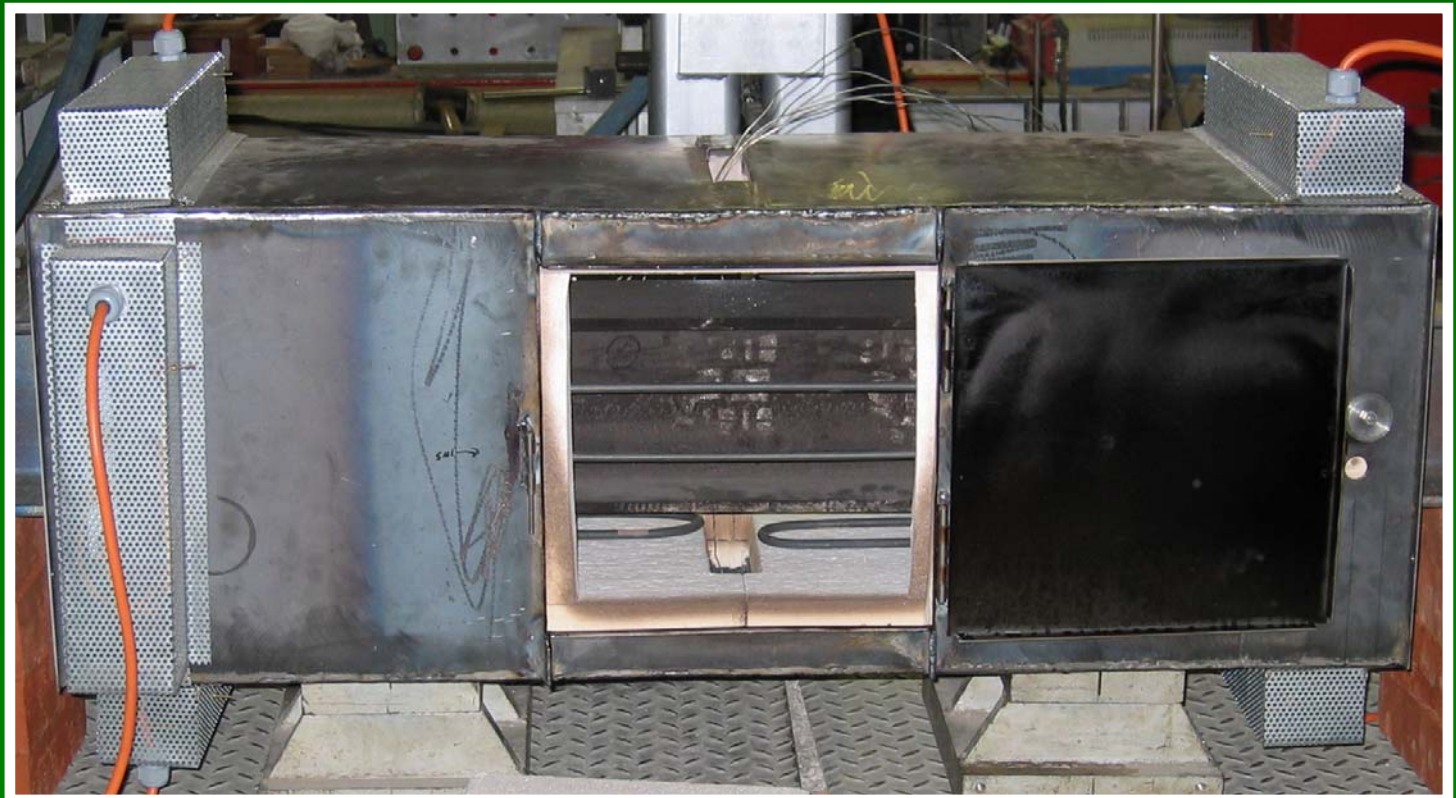
Axial Loading Device

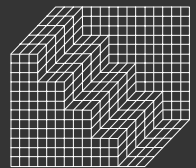
- 500kN hydraulic jack to apply axial load
- Powered by pressure controlled pump to ensure a constant axial load during the heating phase.



Electric Furnace

- Heated by 6 heating elements with a total of 8 kW
- Insulated with 50mm Fibreboard
- Each side is controlled separately to ensure uniform heating of the specimens.





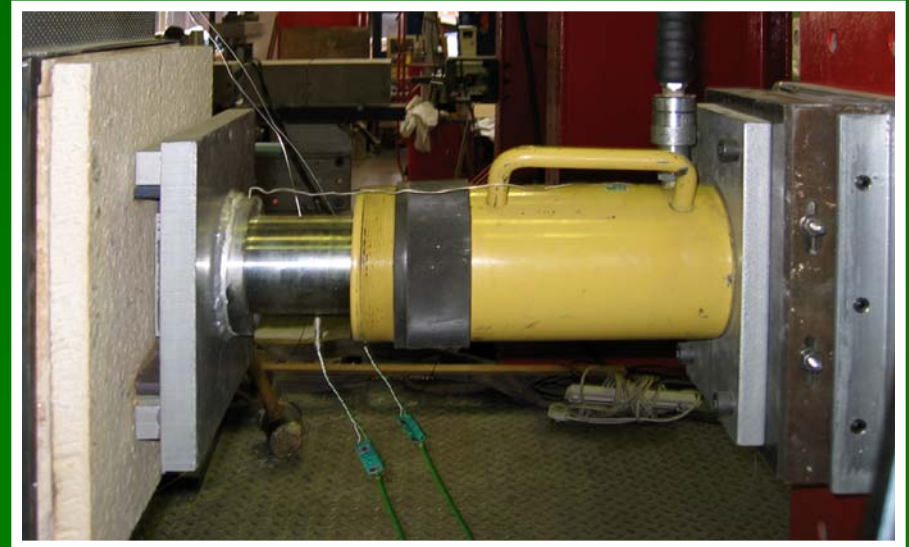
Transverse Loading & Load Introduction

- 500 kN displacement controlled actuator
- Load is introduced via 20mm thick blades to simulate the beam flanges.



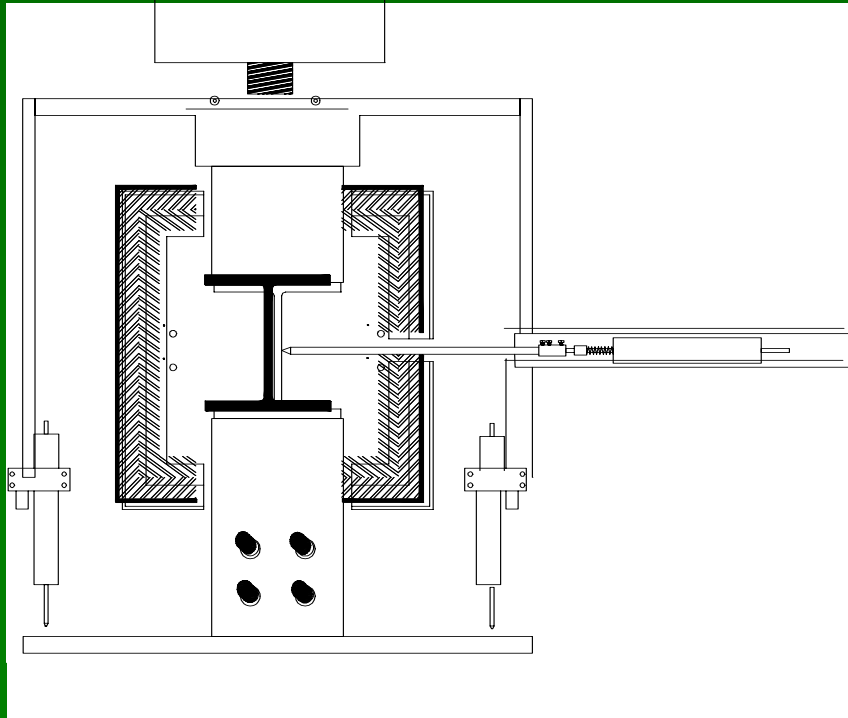
Roller Blocks

- To ensure that all transverse load is reacted by the bottom support and not by the ends, roller blocks are mounted at the ends of the specimen.



Instrumentation

- Steel temperatures are measured by 12 thermocouples.
- 2 LVDTs measure transverse displacement outside the furnace.
- A LVDT fixed to a ceramic rod measures out-of plane deflection of the web.

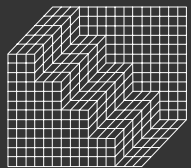


Planned and Conducted Tests



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Axial LR \ Temp	0.0	0.2	0.3
20 °C			✓
450 °C	✓	✓	✓
550 °C	✓	✓	✓
600 °C		✓	

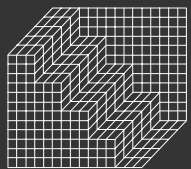
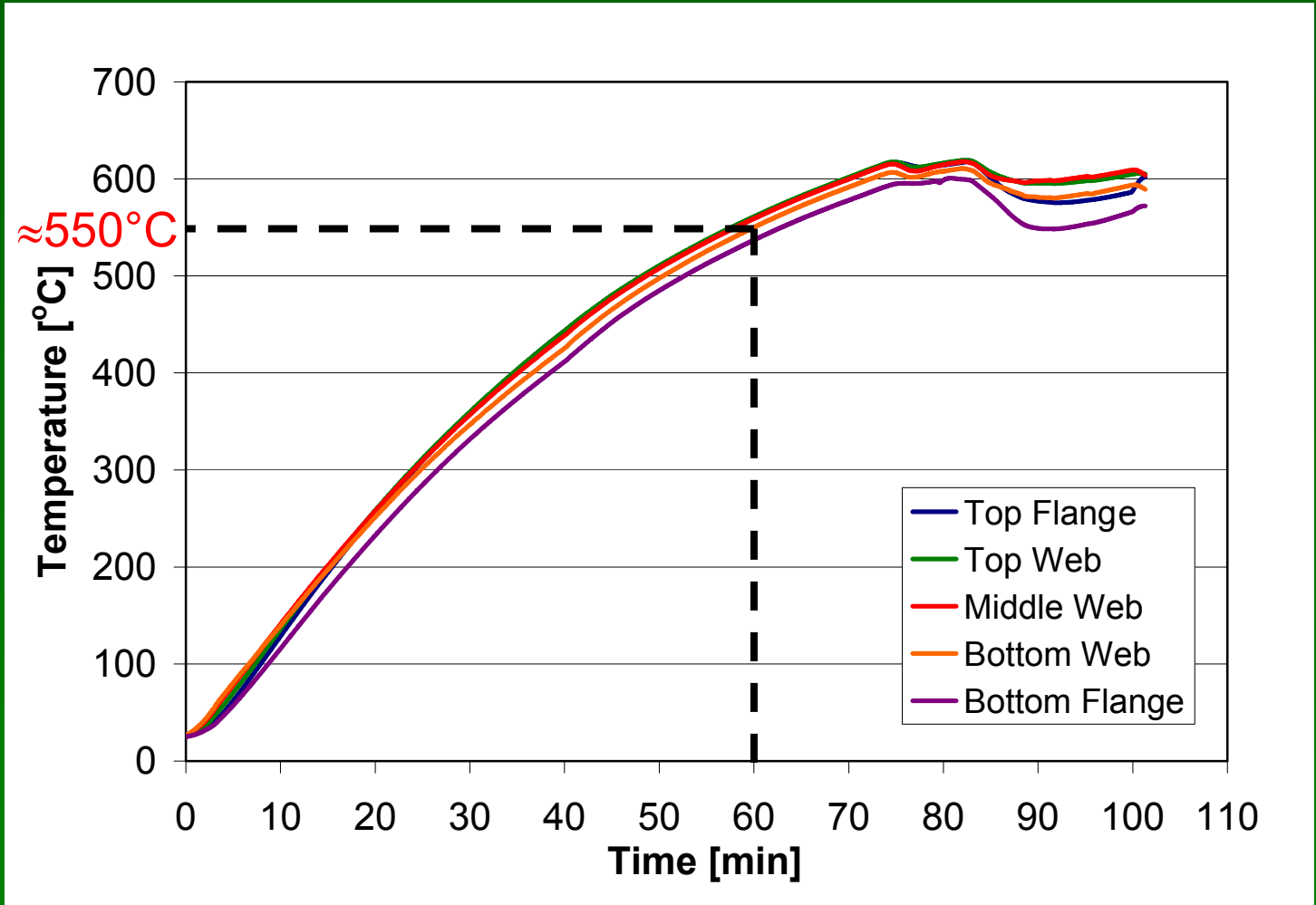


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Typical Time-Temperature curves

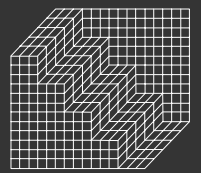
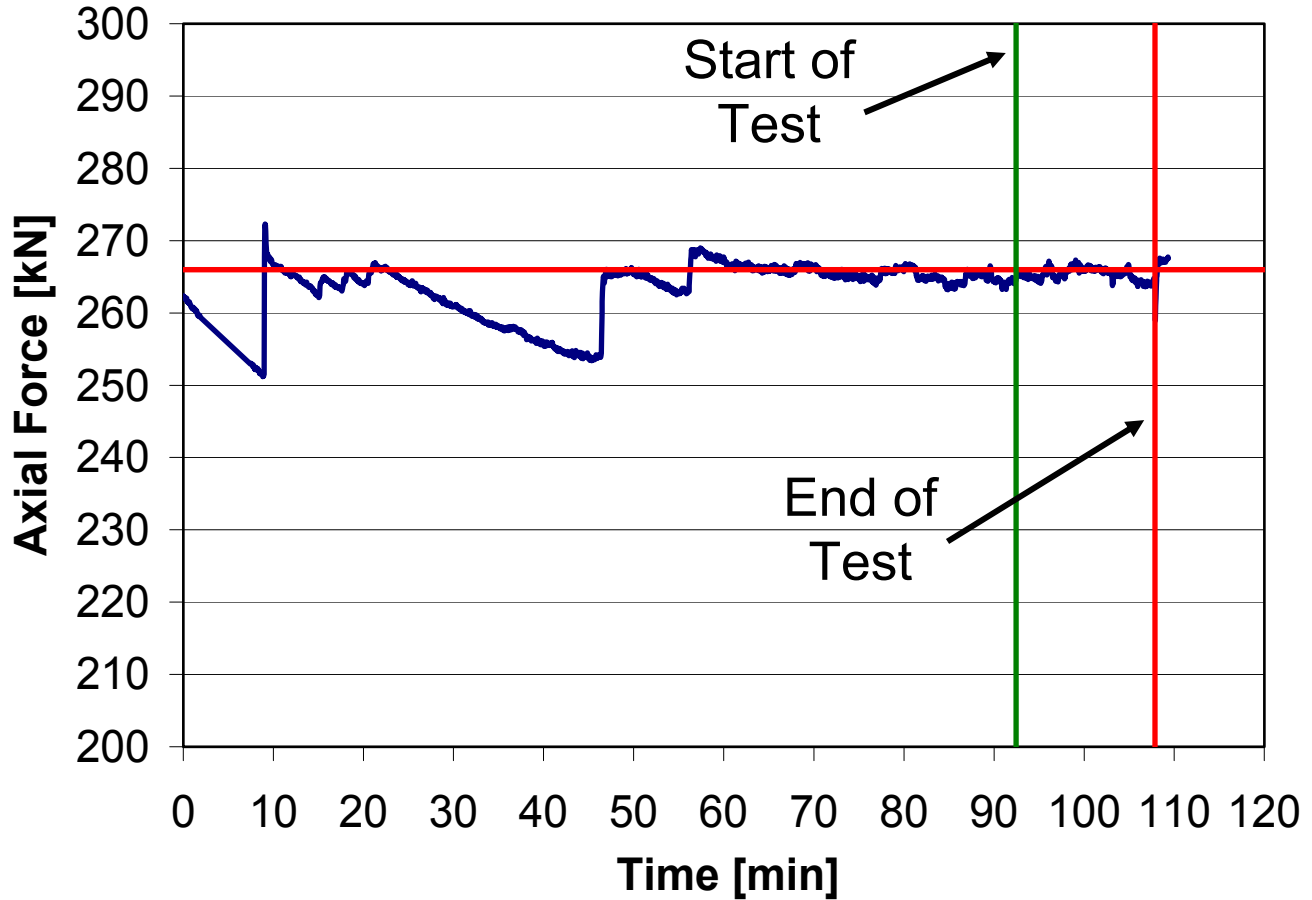


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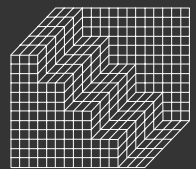
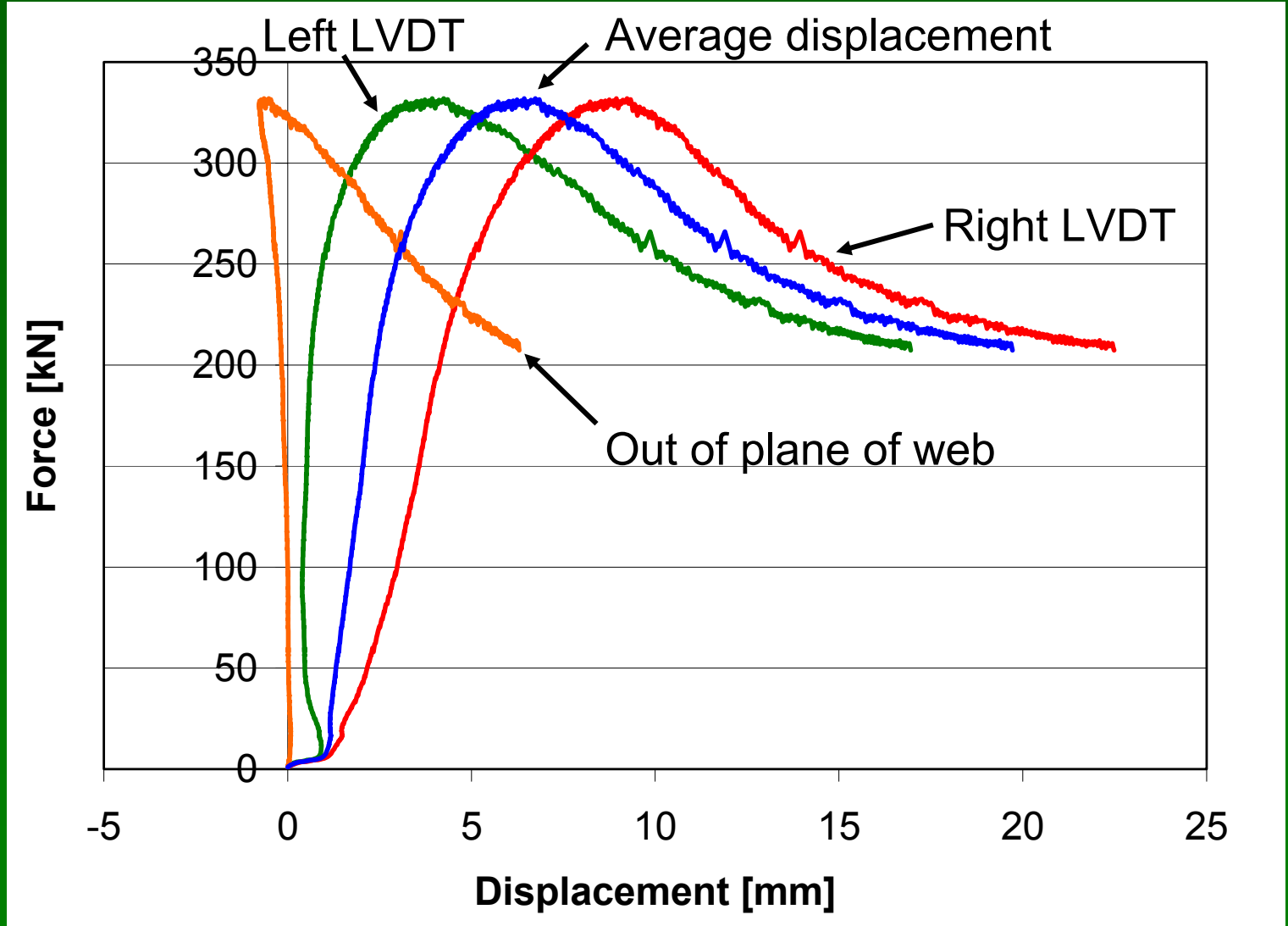


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Axial Load in the Specimen



Typical Transverse Displacement

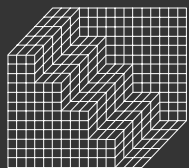


Summary of the Conducted Tests



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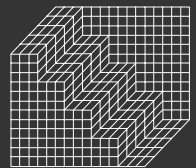
Test #	Web temp.	Flange temp.	Axial load N	Axial load ratio $N/N_{pl,1.0\%}$	F_u	d_u
	[°C]	[°C]	[kN]	[-]	[kN]	[mm]
3	20	20	394	0.3	413.7	6.4
6	20	20	398	0.31	423.4	7.5
4	450	424	3	0.00	331.7	5.0
1	453	440	266	0.23	331.0	5.9
7	458	429	403	0.36	331.4	5.4
2	515	482	390	0.40	280.0	4.6
5	531	516	268	0.29	246.4	6.8
8	549	513	2	0.00	257.4	6.0
9	591	562	266	0.39	175.1	6.4



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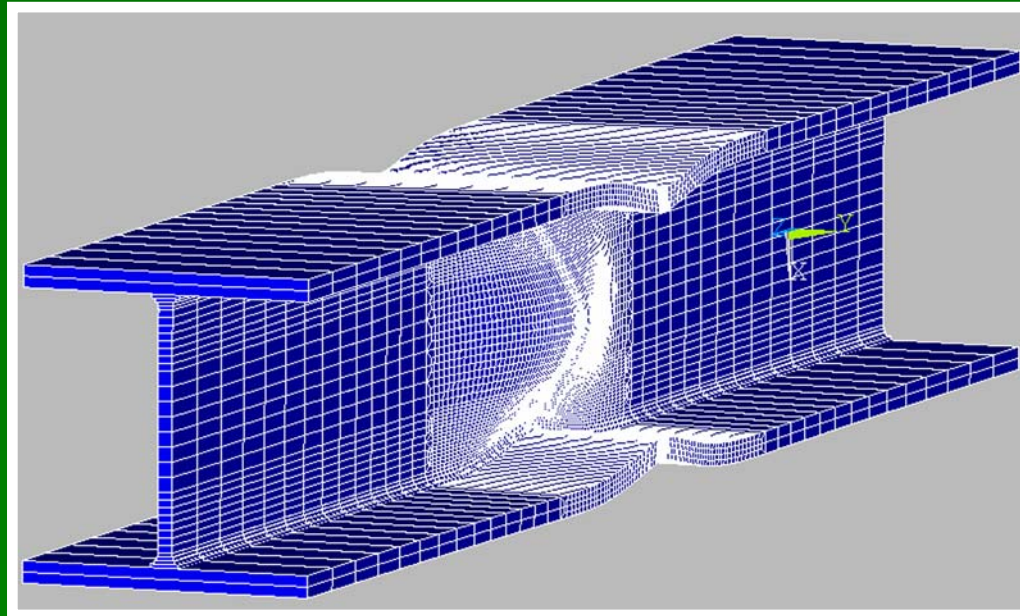
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Comparison between Experiments and FEM-Model...

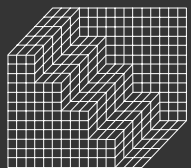
Deformed Shapes of Tests vs. FEM



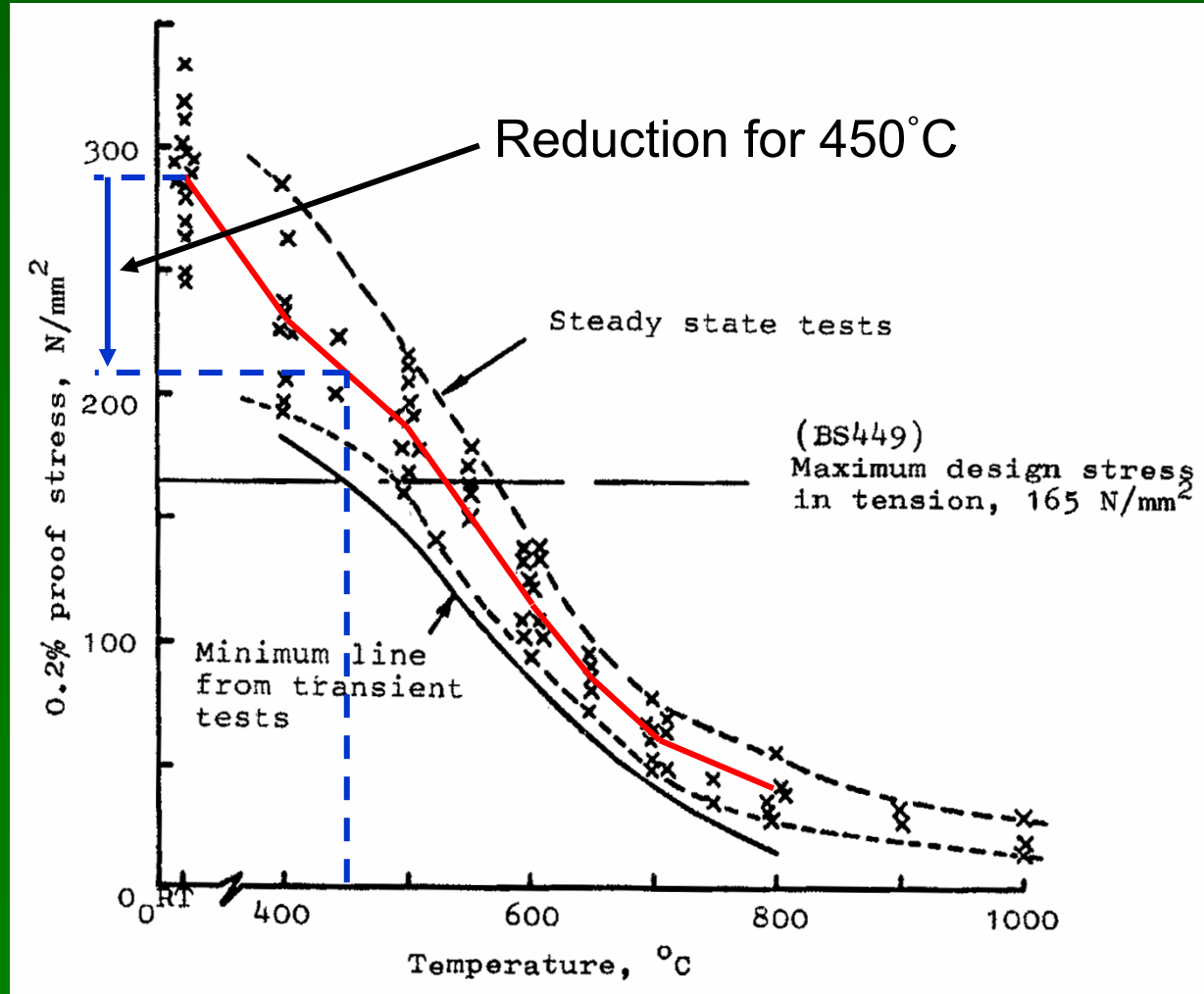
Material Curves for Steady-State Tests

- The high temperature material model in EC 3 Part 1.2 is based on the transient tensile tests.
- Thermal creep effects are included, which are marginal in steady-state experiments.
- No strain-hardening above 400°C is considered.
- To model steady-state experiments realistically the EC3 material model can not be used.

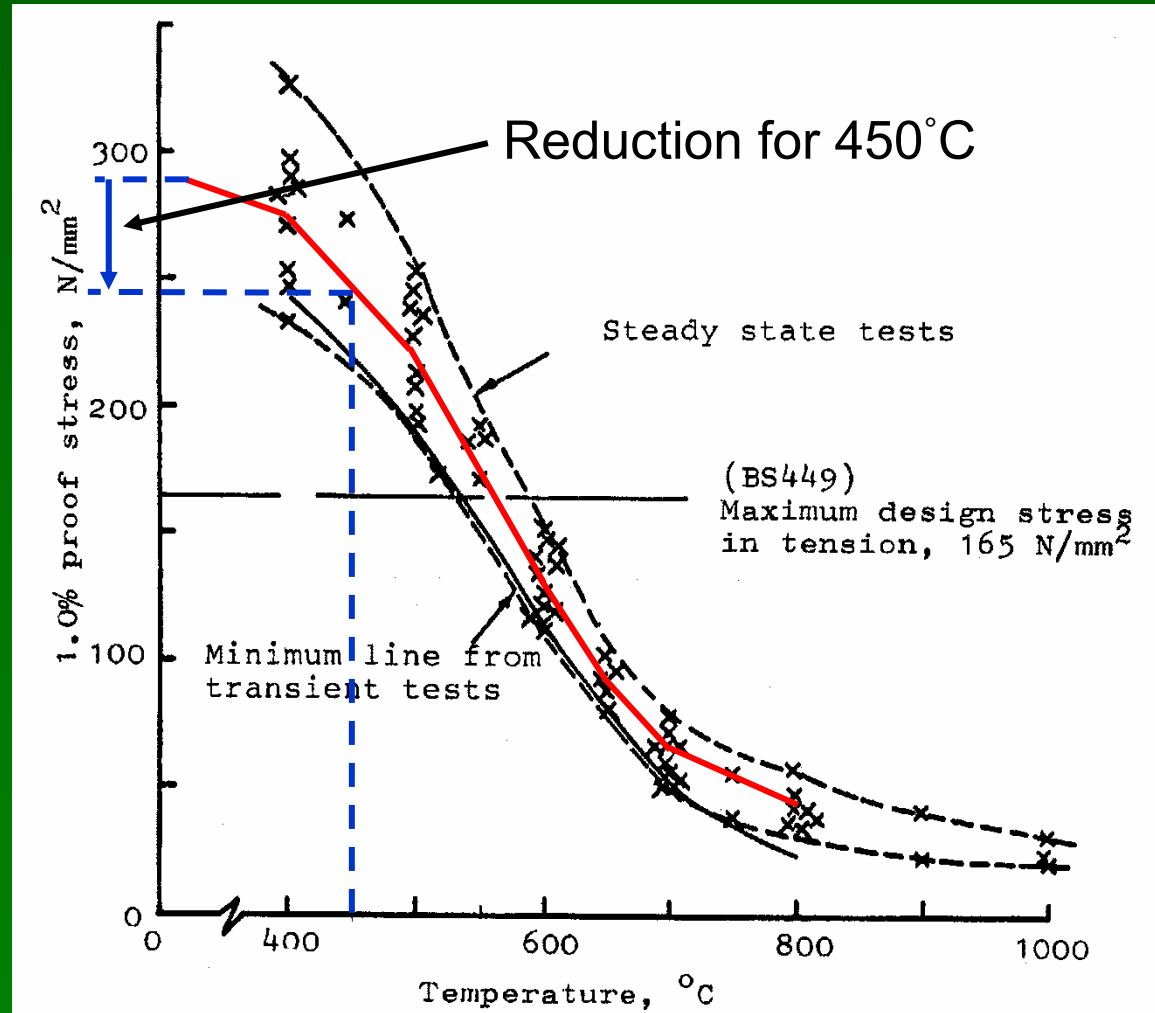
A new material model has been developed based on the steady-state tensile tests by Kirby and Preston.



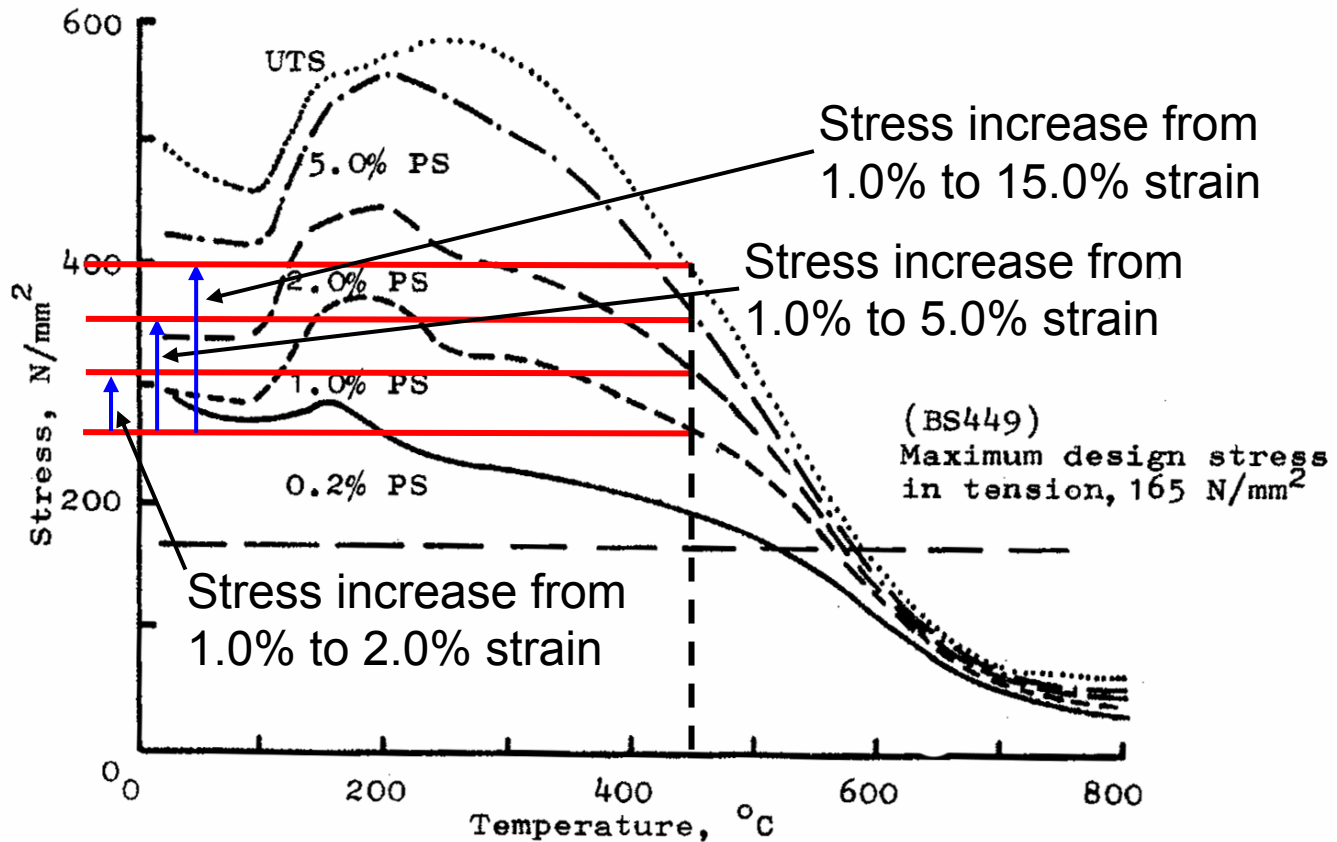
Reduction of the Stress at 0.2% Strain



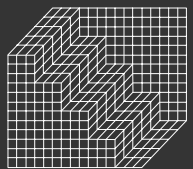
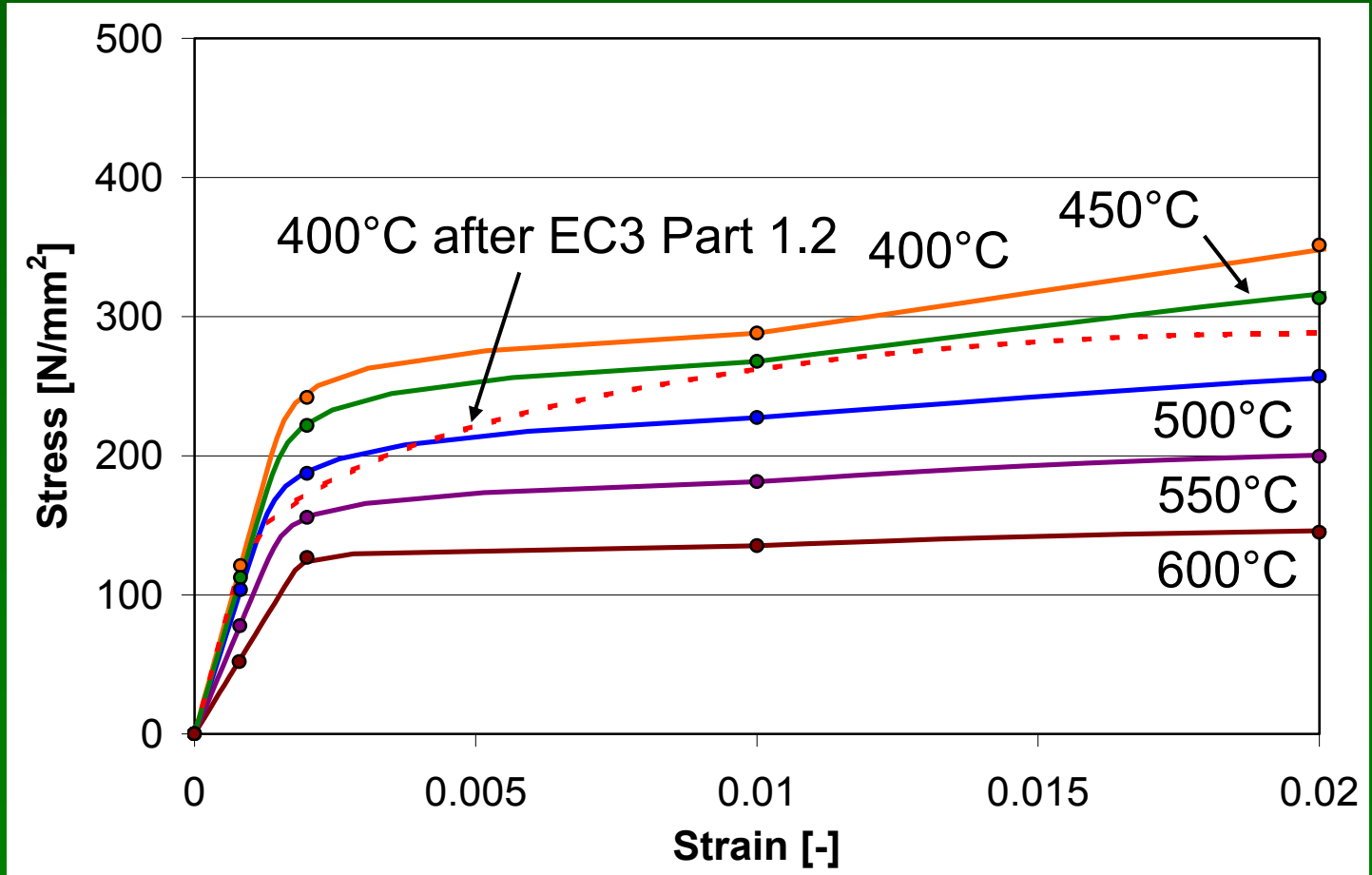
Reduction of the Stress at 1.0% Strain



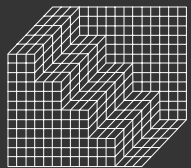
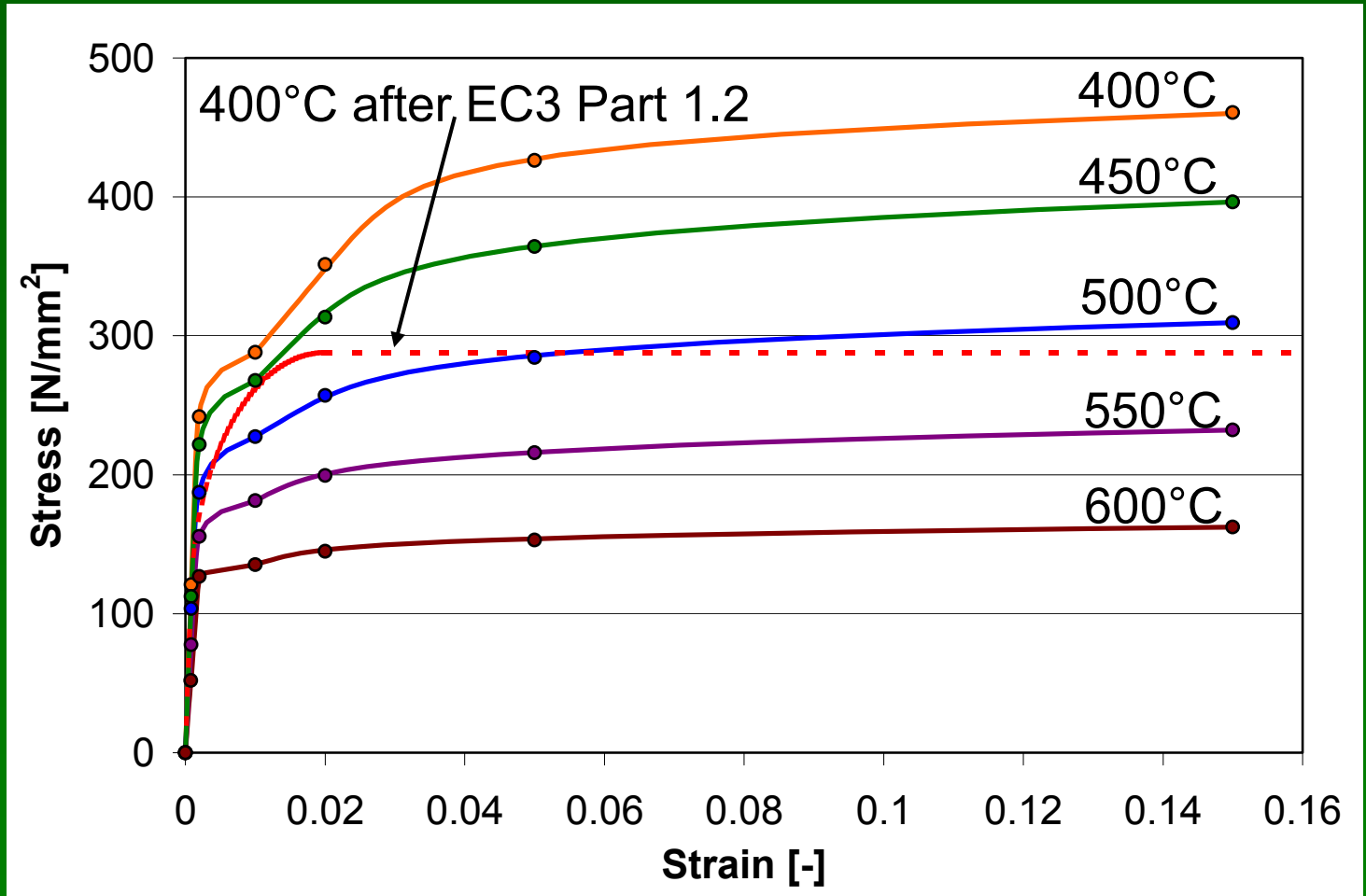
Reduction of the Strain Hardening



Material Curves for Steady-State Tests

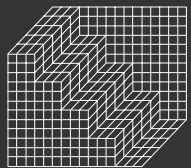
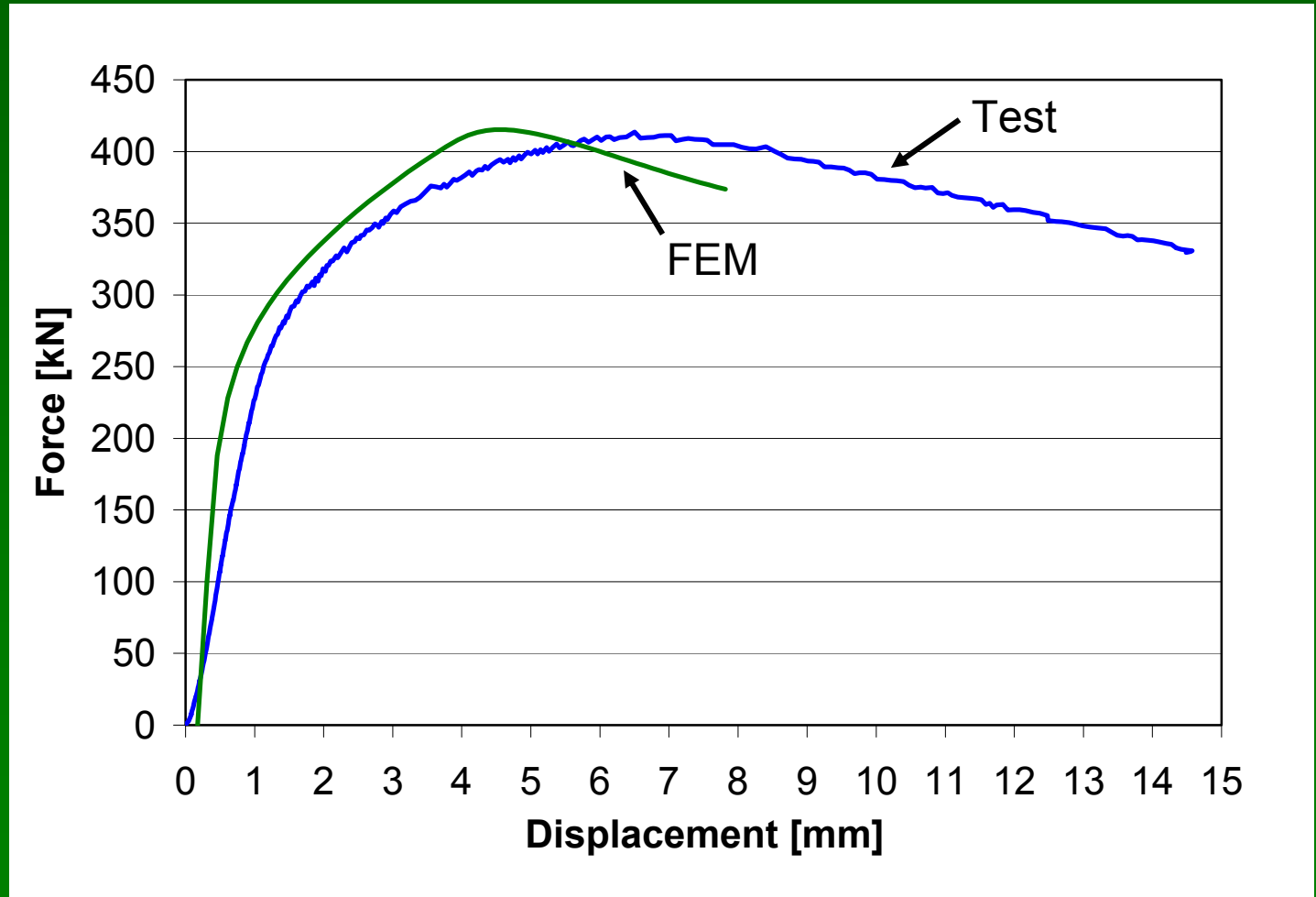


Material Curves for Steady-State Tests



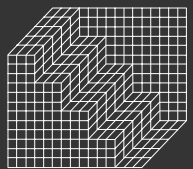
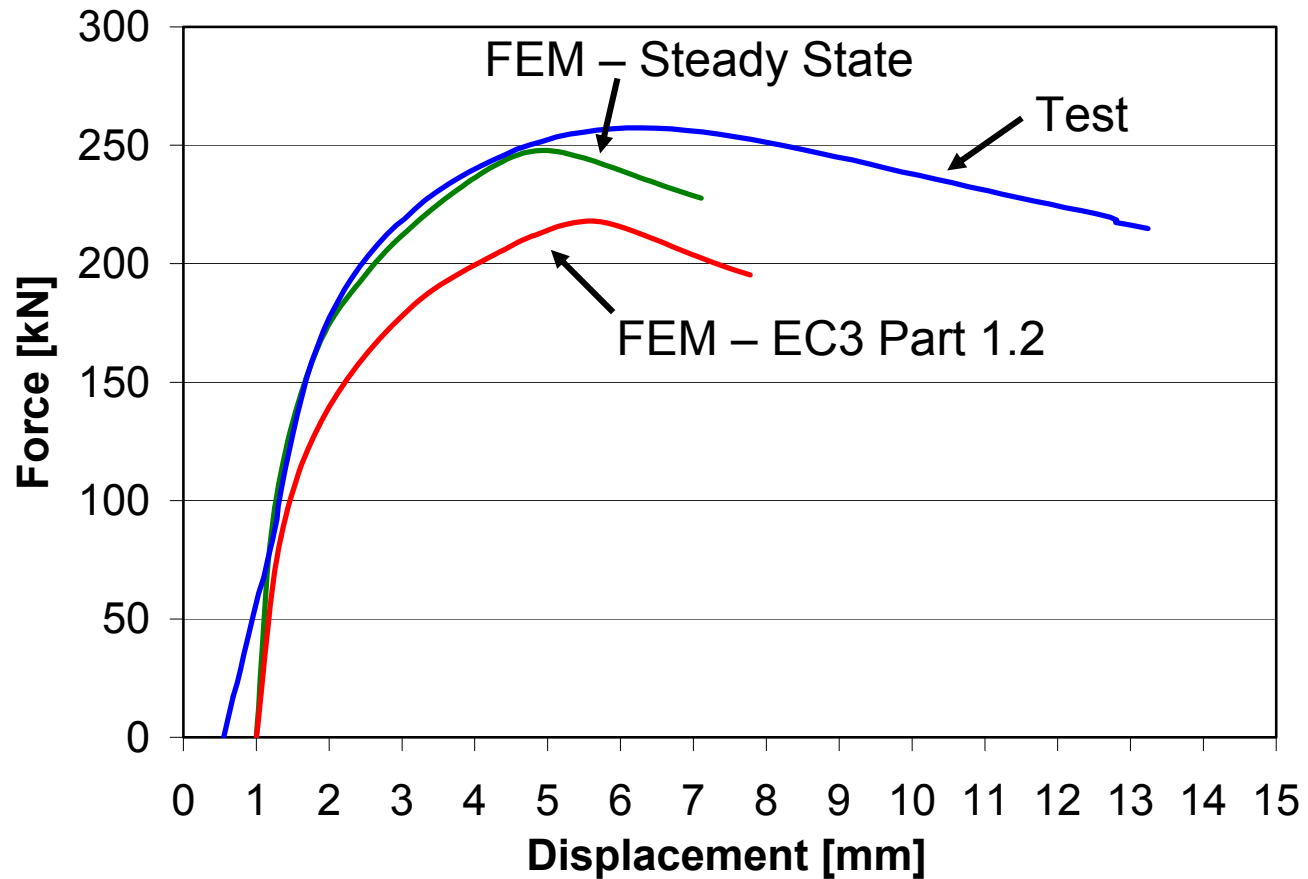
Comparison Test – FEM

Test #: 3 – Temp.: 20°C – Axial load: 394kN



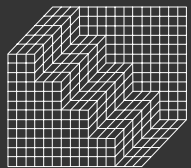
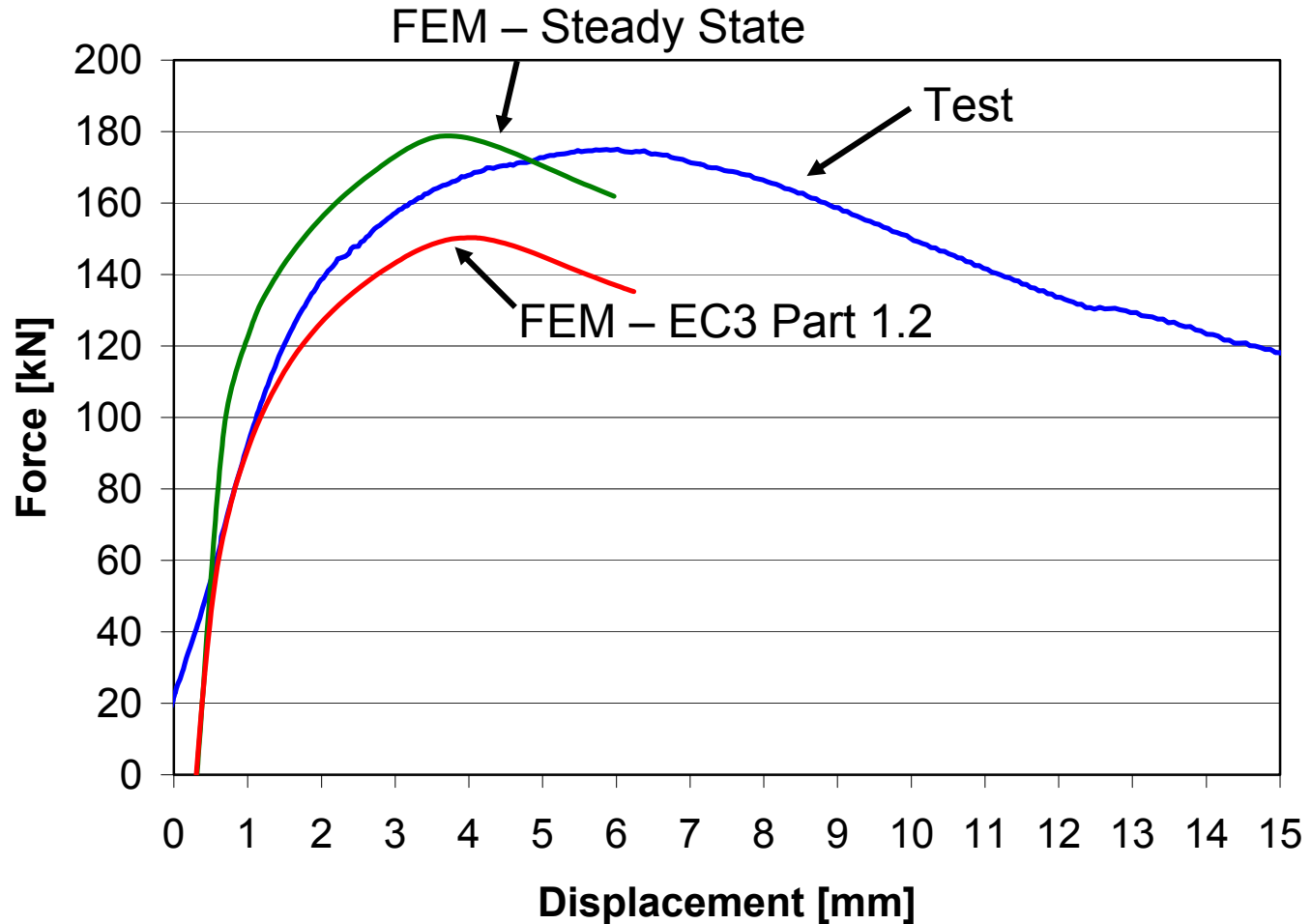
Comparison Test – FEM

Test #: 8 – Temp.: 549°C – Axial load: 2kN



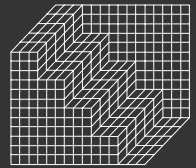
Comparison Test – FEM

Test #: 9 – Temp.: 591°C – Axial load: 266kN





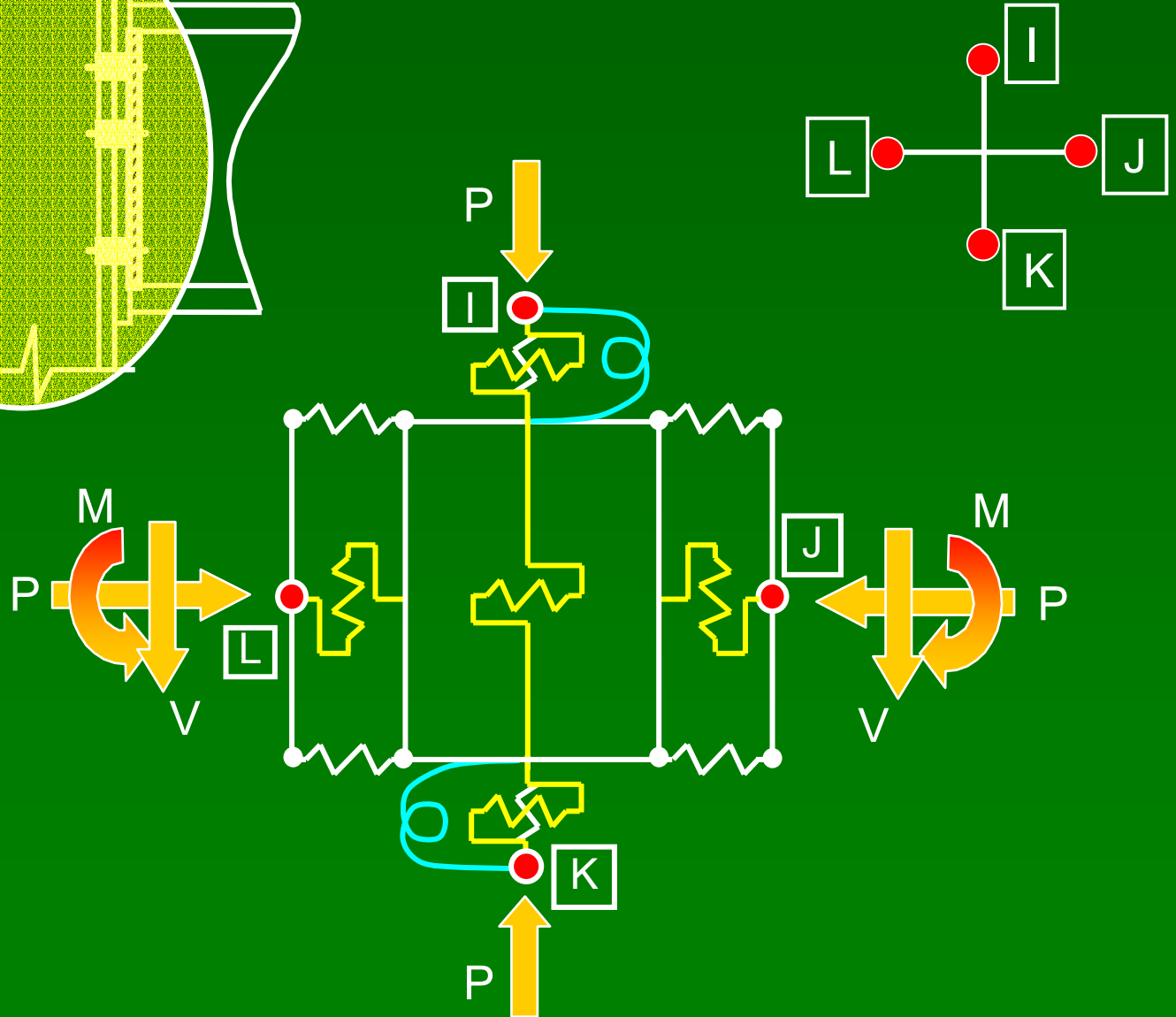
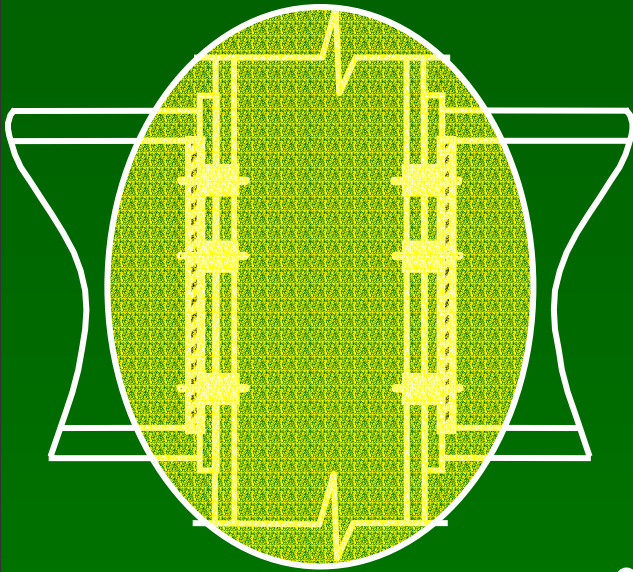
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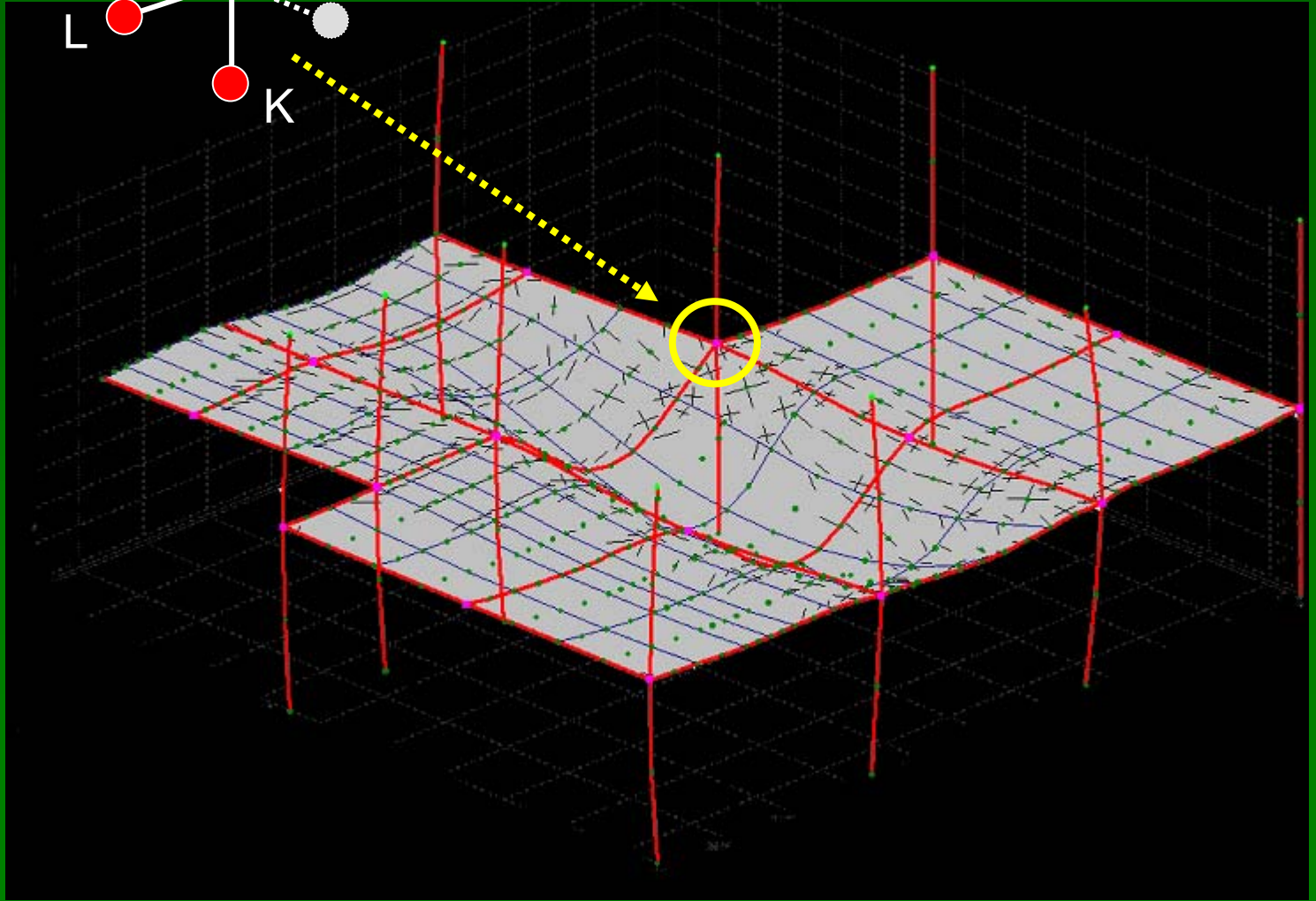
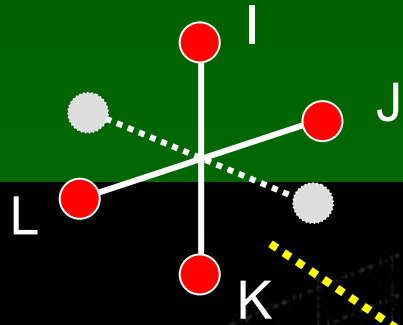
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Practical Application...

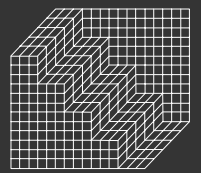
High-temperature component-based joint finite element



Implementation of the element in VULCAN



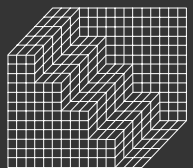
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Conclusion

- To predict the behaviour of joints in fire a flexible approach like the component method is required.
- Each component needs to be analysed at elevated temperatures.
- For the compression zone a workable approach for elevated temperatures has been developed.
- Material curves to model steady-state experiments have been derived.
- The Component Method together with VULCAN gives a feasible way to include realistic joint behaviour in the global analysis of structures in fire.

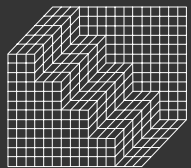


What is next?

- Finish the experimental study.
- Do more FEM-modeling for a wider understanding of the compression zone.
- Revise the simplified model and the reduction factors.
- Assemble component based joint element.
- Run whole composite frame analysis with VULCAN.



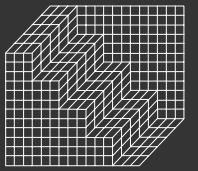
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Joint Component Behaviour in Fire

Questions ..?

Florian M. Block

Steel in Fire Forum

Rotherham, UK

September 2004